

4th Round Table on MNT for Space
20/22 May, 2003 (ESTEC, Noordwijk, NL)



RF-MEMS metal contact capacitive switches

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*4th Round Table on
Micro/Nano Technologies for Space
ESTEC Conference Centre, Noordwijk, The Netherlands 20/22 May 2003*

SEEDS FOR
TOMORROW'S
WORLD



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OUTLINE

Introduction

- Target specs
- Configurations and choice

Capacitive RF-MEMS switches

- Top floating metal (→"metal contact" capacitive switch)
- Boosted switch

0-level packaging

- Technology
- RF performance

Reliability

Conclusions

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Target specifications RF-MEMS switch for communications switching matrix

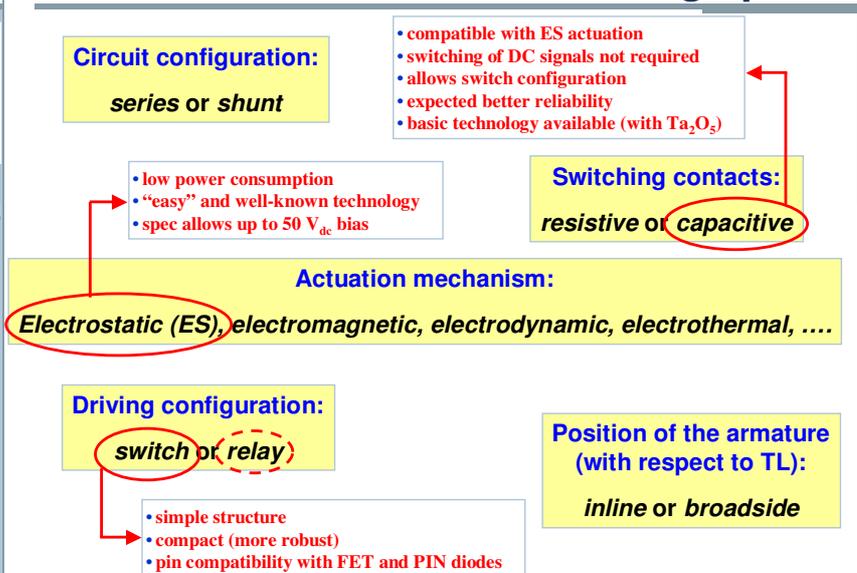
- n Frequency range 1-30 GHz
- n Insertion loss < 0.4 dB
- n Isolation > 50 dB
- n Return loss > 20 dB

- n Actuation voltage < 50 V
- n Switching time “small”
- n Power consumption “minimal”

- n Operating ambient -25 to +75 °C
- n Life time 10⁶ cycles

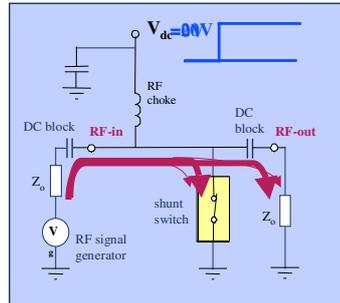
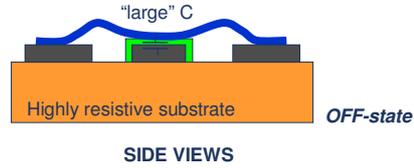
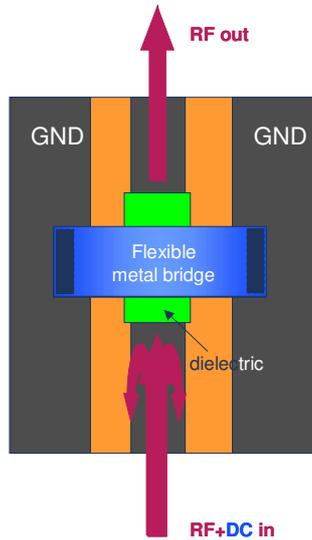


Configuration & Choice of switching device meeting specs





TOP VIEW



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Shunt capacitive RF-MEMS switch implemented on a CPW line

It is the capacitance ratio that counts:

$$IL < IL_{spec} \text{ AND } I > I_{spec}$$

in the frequency band $\langle \omega_l, \omega_u \rangle$ requires that:

$$r \equiv \frac{C_{down}}{C_{up}} > \frac{\omega_u}{\omega_l} \sqrt{\frac{10^{0.1I_{spec}} - 1}{10^{0.1IL_{spec}} - 1}}$$

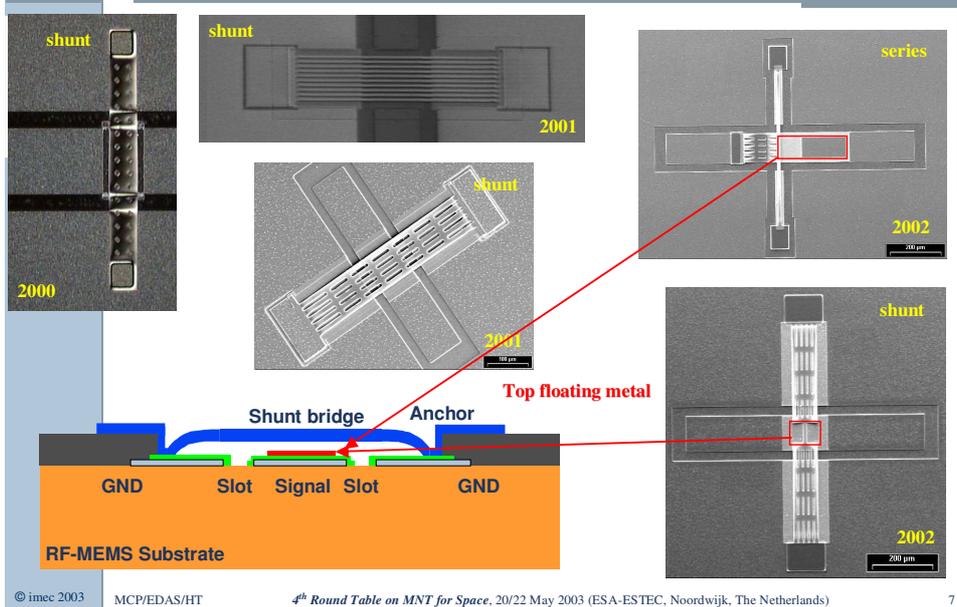
Switch modeled as lumped capacitor
 Applies for series and shunt switches

Capacitance ratio determined by process (not geometry):

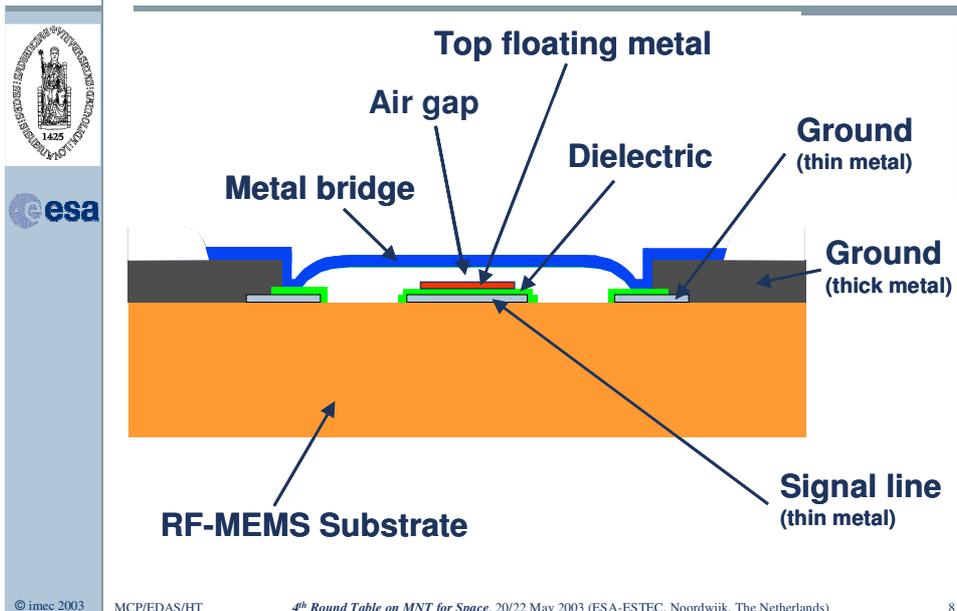
$$r \equiv \frac{C_{down}}{C_{up}} = \frac{\epsilon_r d_o}{d \epsilon} \quad \text{Conventional capacitive switch}$$



RF-MEMS *electrostatically actuated capacitive switches* at IMEC

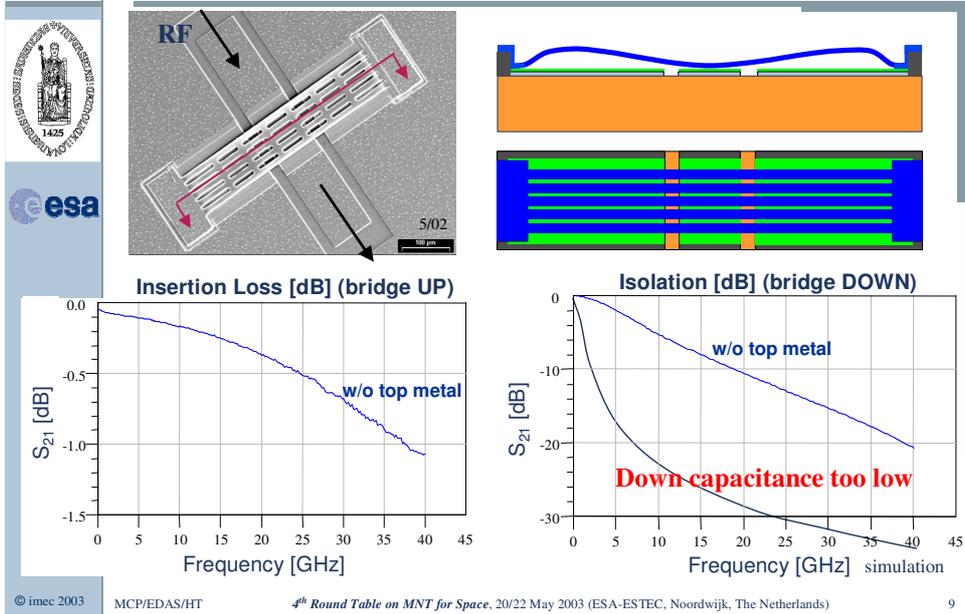


5/6-Mask Fabrication Process "Metal Surface Micromachining"

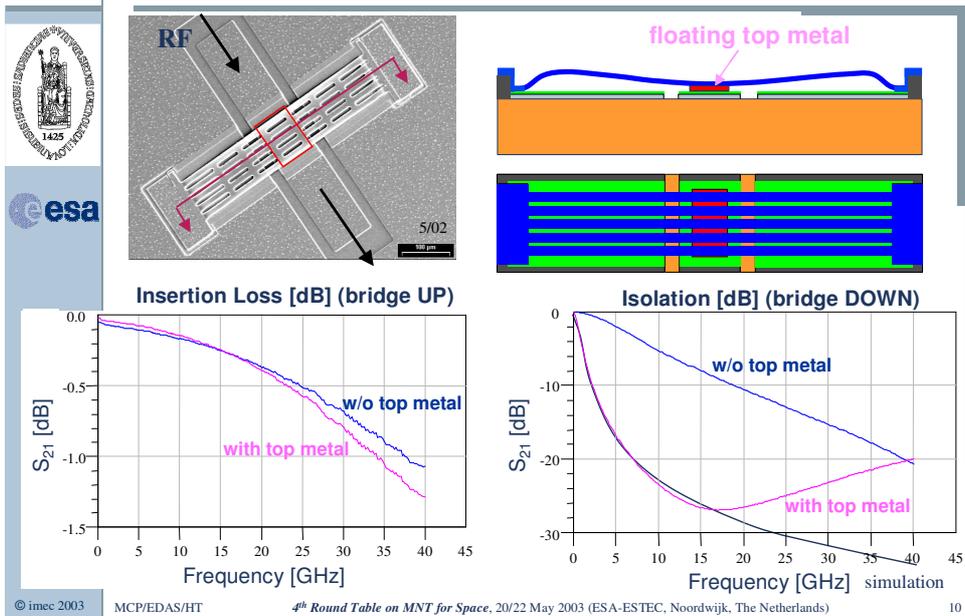




ES actuated capacitive shunt switch:

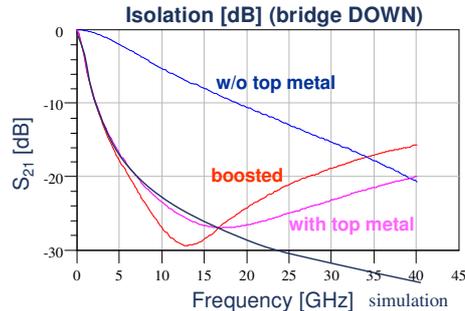
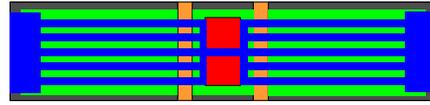
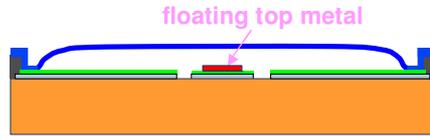
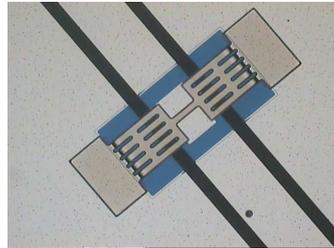


ES actuated capacitive shunt switch: Introduction floating top metal





ES actuated capacitive shunt switch: Introduction floating top metal & “boosted” switch



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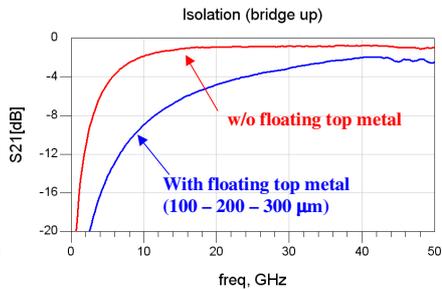
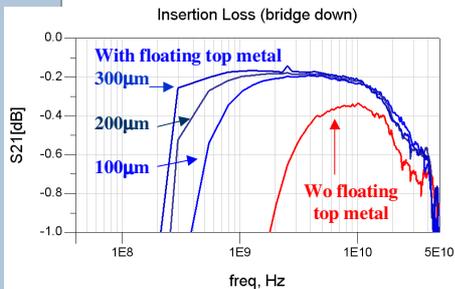
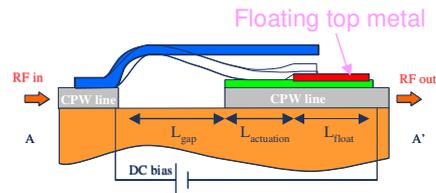
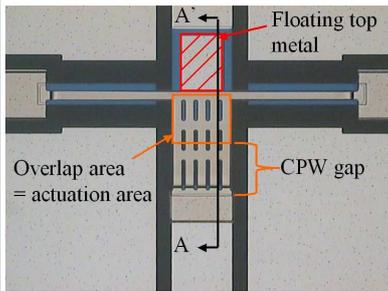
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ES actuated capacitive series switch: Introduction floating top metal & “boosted” switch



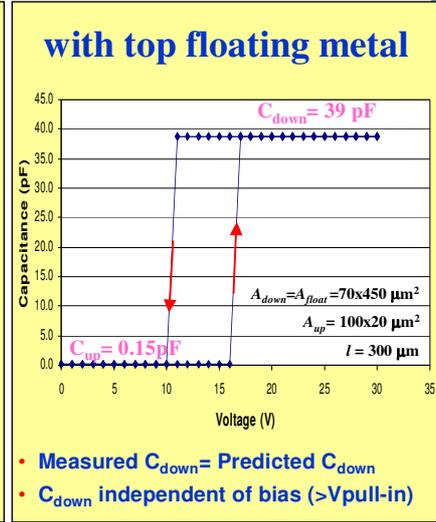
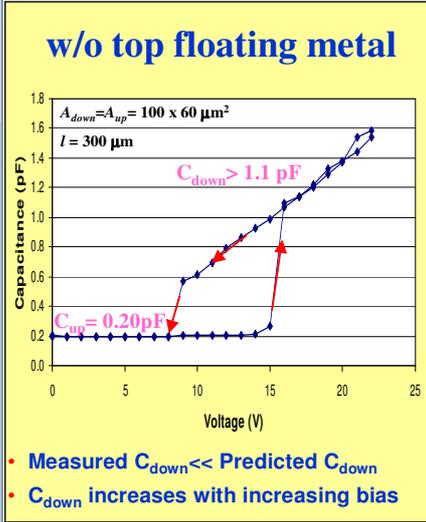
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C-V measurements shunt switch The floating metal makes the difference



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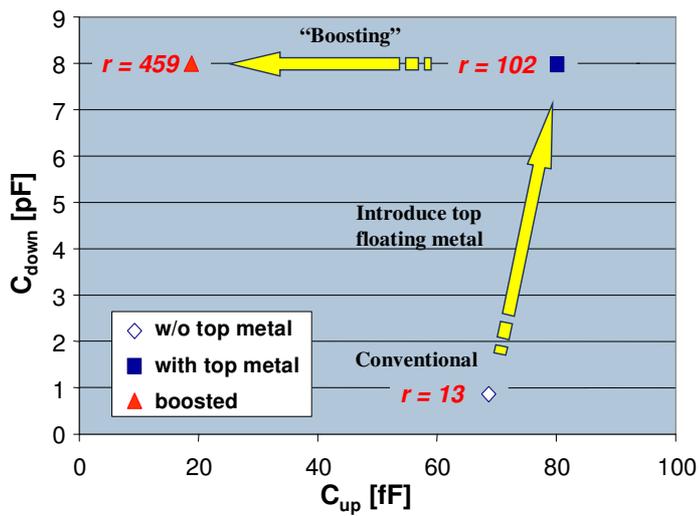
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The road to a high $r = C_{down}/C_{up}$ ratio



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Conclusions (1): The trick of the *top floating metal*

n Down capacitance C_{down} is predictable and is accurately defined by the area of the top floating metal:

$$C_{down} = \frac{\epsilon_r A_{float}}{d_\epsilon}$$

n Area in the down state A_{down} can be chosen “independent” from the area in the up state A_{up} and from the actuation area A_{act} :

$$A_{down} = A_{float} \neq A_{up} \approx A_{act}$$

n Area difference in up and down state can be used to amplify the capacitance area r (boosted concept):

$$r \equiv \frac{C_{down}}{C_{up}} = \frac{\epsilon_r d_o}{d_\epsilon} \cdot \frac{A_{float}}{A_{up}}$$

ratio for conventional capacitive switch “BOOSTING Factor β ”

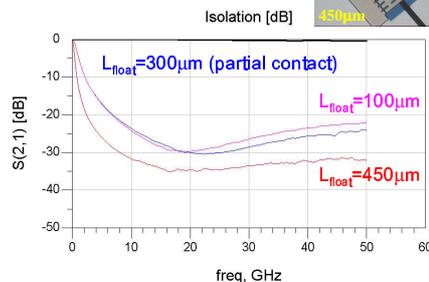
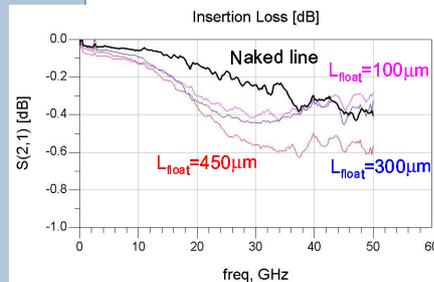
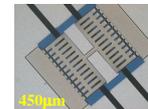


Broadband switching (1-30 GHz)

A. Single switch:

- n IL < 0.4dB and I > 50dB over 1-30 GHz requires down/up capacitance ratio r of: $r = C_{down}/C_{up} > 30,000$ (“impossible” for conventional technology)
- n For a switch technology with $\epsilon_r = 25$, $d_o = 2.5\mu\text{m}$, $d_\epsilon = 0.2\mu\text{m}$, the capacitance ratio is $r \approx 300$. **boosted design** requires a boosting factor $\beta > 100$ (e.g. if $A_{up} = 20 \times 20\mu\text{m}$, then $A_{float} = 4 \times 10^4 \mu\text{m}^2$, or for $W_{float} = 70\mu\text{m}$, $L_{float} > 0.6\text{mm}$)

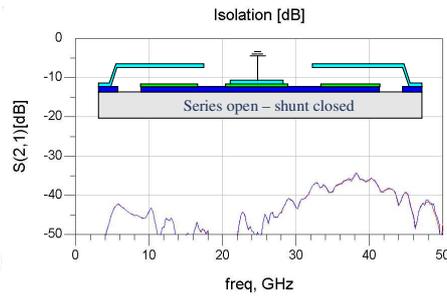
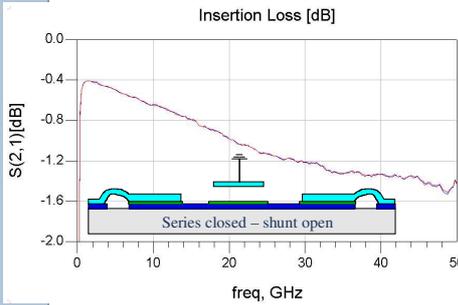
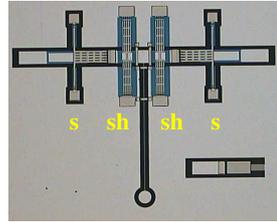
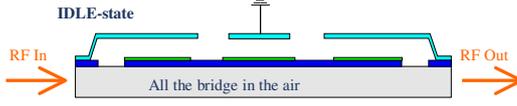
Is feasible





Broadband switching (1-30 GHz)

B. Combination switch: Series-shunt-shunt-series (with boosted constituents)



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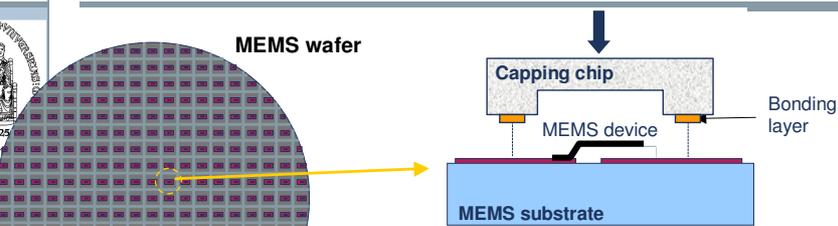
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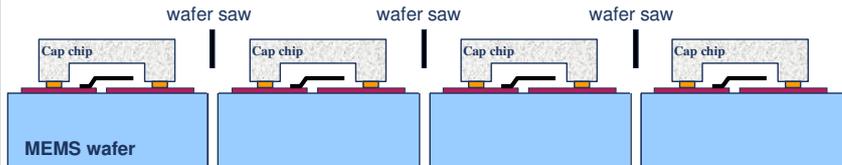


Need for on-wafer MEMS packaging



Standard wafer sawing will destroy fragile MEMS
 Needed for *on-wafer* protective envelope

➔ **0-LEVEL PACKAGE**



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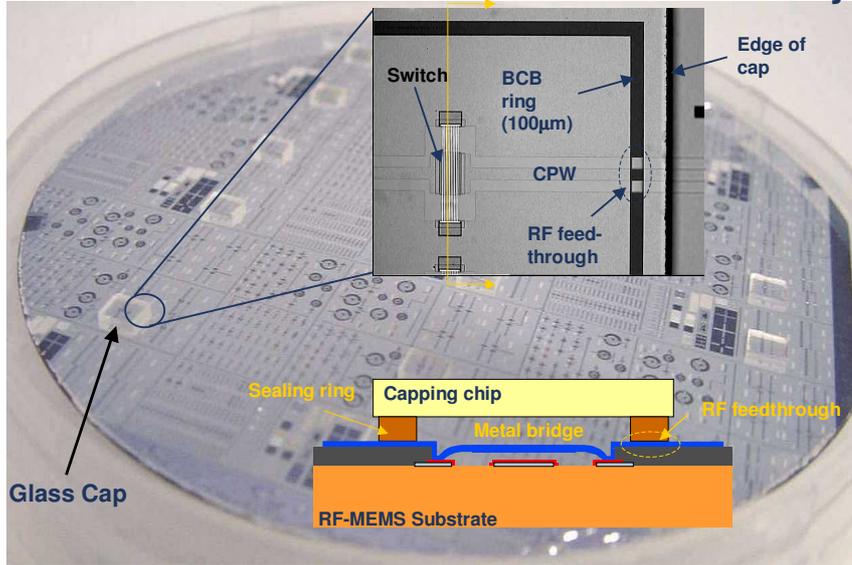
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0-level packaged RF-MEMS switches C2W assembly



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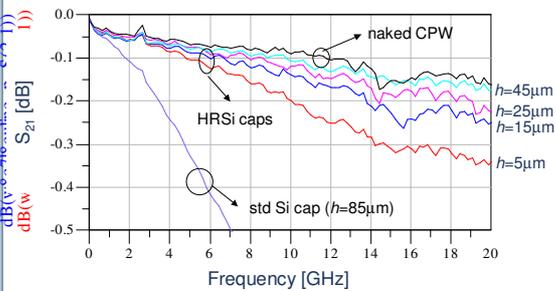
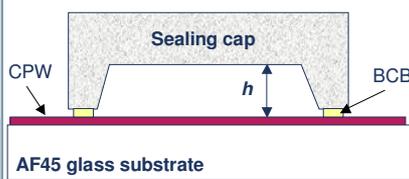
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Influence of the cap material and cavity height (planar feedthrough)



CPW:
 (25/100/25µm
 Cu 3µm thick
 2.3 mm long)
AF45 substrate
Cap material:
 standard Si (1-10Ωcm)
 HRSi (>4000Ωcm)
 BCB bond (5µm thick)

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Conclusions(2)

- n The implementation of the top floating metal is an easy and viable way to build capacitive switches with predictive RF (and C-V) characteristics.
- n The boosted capacitive switch approaches the behaviour of the resistive relay, while retaining the advantageous features that are characteristic for a switch configuration (compact, simple, "two-terminal device").
- n The specifications $IL < 0.4\text{dB}$ and $I > 50\text{dB}$ requires a capacitance ratio better than 30,000; this seems feasible for a single switch, but the ultimate limitation of satisfying the spec is the parasitic resistance and inductance in series with the switch capacitance.
- n Combination switches improve the RF specifications compared to a single switch design, but this goes at the expense of a higher complexity, increased size (implying higher resistive losses).
- n The influence of the 0-level package on the RF characteristics can be kept negligibly small.
- n **Critical issues remaining to be solved are:**
 - n packaging (hermeticity, controllability, cost)
 - n reliability (stiction, life cycles, choice of materials)



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