

# Micro-Mirror-Arrays for Adaptive Optics in Space

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Werner Hupfer, EADS Astrium GmbH

Dr. Andreas Gehner, FhG-IPMS

Jan Liesener – ITO

Kotska Wallace – ESA-ESTEC

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# Introduction – Project Organization

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**ESA Contract Nr. 16632/02/NL/PA**



**EADS Astrium GmbH**

Project Management, System Engineering, Technical Specifications, Simulation



**FhG–IPMS (Fraunhofer Gesellschaft - Institut for  
Photonical Microsystems)**

MMA Design and Manufacturing



**ITO (University of Stuttgart, Institut for Technical  
Optics)**

Fibre Coupling Concepts, Breadboard Design,  
Realization, Tests

## Introduction – Background/Motivation

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Large optical telescopes for space applications will require light-weighted, possibly segmented primary mirrors in order to reduce mass and cost.

But extreme light-weighting introduces wave-front errors caused by its floppiness mainly due to:

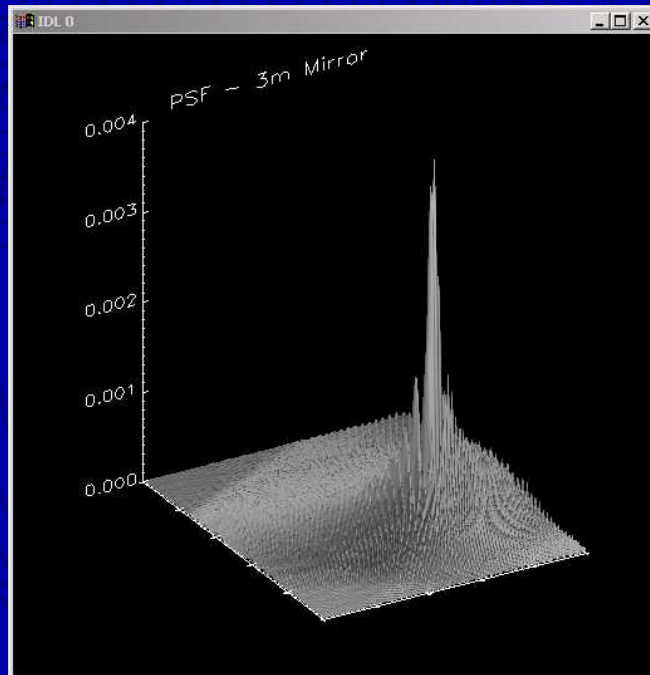
- print-through from mirror polishing
- mounting stress
- gravity release from transition to Zero-G
- asymmetric and periodical heating in Earth orbit
- discontinuities between segments

**In order to produce diffraction limited performance  
Wavefront Correction with Adaptive Optics (AO) is required!**

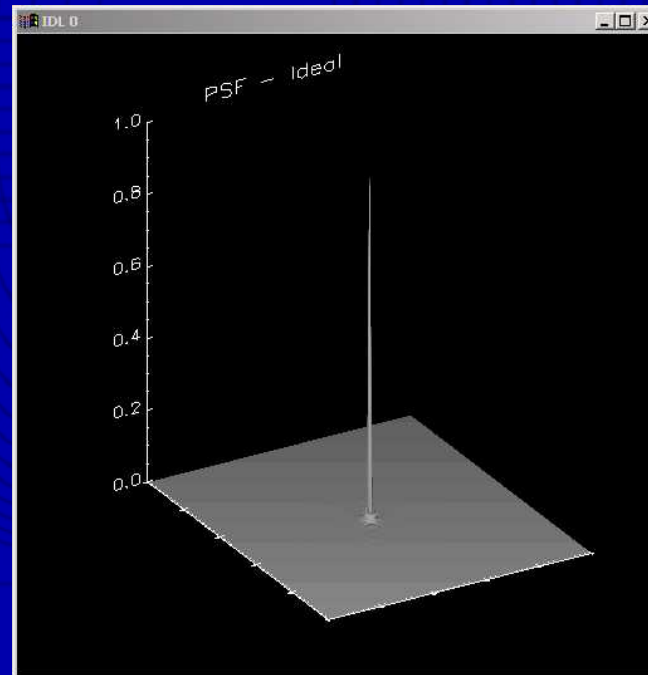
# Introduction – Background/Motivation

## Comparison of Star-Images:

Typical distortions of 3m light-weighted mirror



Corrected with AO



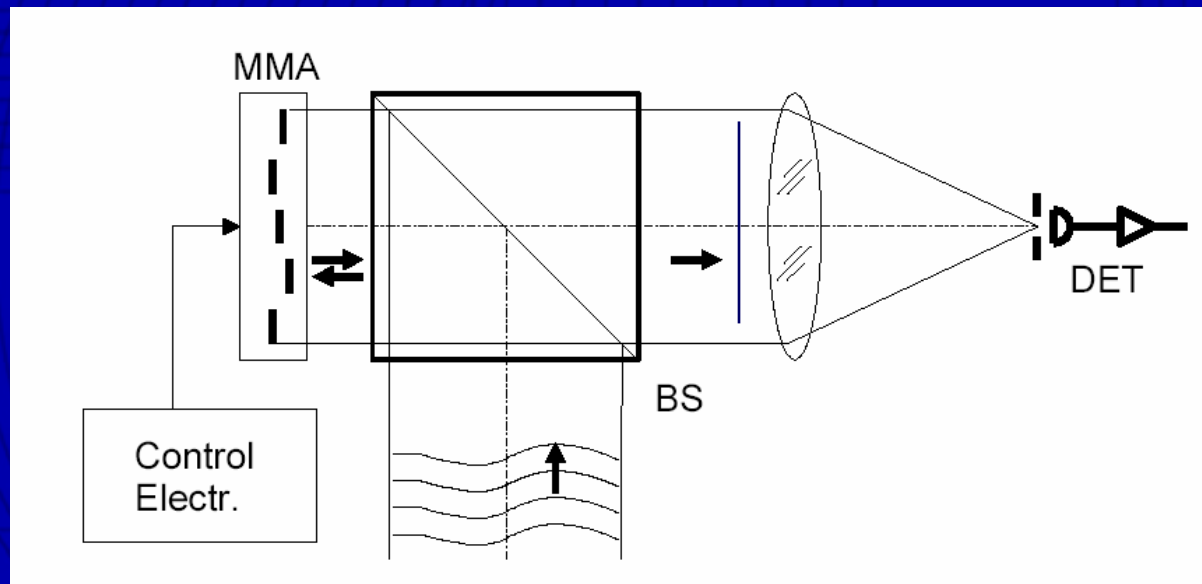
Energy is spread out over large area.  
Peak is a fraction and not centred.

# Introduction – Background/Motivation

## Principle of **Wave-front Correction**:

Correction can be directly

- at main mirror
- or further down the optical chain, where beam size is smaller.



Correction-Device (MMA) has complementary 'shape' of incoming distorted wavefront. Wavefront reflected from MMA is almost flat.

## Introduction – Project Objective

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Demonstrate and analyse the wave-front correction capability of two types of Micro-Mirror-Arrays within an application:

- Coupling of a distorted free-space laser beam into a mono-mode optical fibre (Space application example: optical satellite communication)

Investigate various types of wave-front aberrations/distortions:

- typical wave-front errors of a light-weighted mirror
- positional misalignments of individual segments of a segmented mirror (step errors)

## MMA – Characteristics and Parameters

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**Why MMAs:** MMAs are new promising and already commercially available wave-front correction devices based on MEMS technology. They provide high spatial resolution. The mirrors are individually addressable and have fast switching times.

Two types of MMAs were designed and manufactured by FhG-IPMS, then investigated and tested in a breadboard setup:

- Piston-Mirror MMA
- Tilt-Mirror MMA

Number of Mirrors:	240 x 200
Mirror Pitch (Size):	40(35) x 40(35) $\mu\text{m}$ 9.6 x 8 mm
Piston Mirror max. Stroke:	~ 400 nm (8 bit resolution)
Tilt Mirror Tilt Angle:	1° - used in binary operation

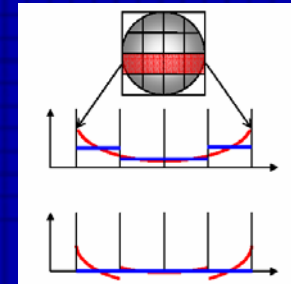


# Wavefront Correction with MMAs

## Principle:

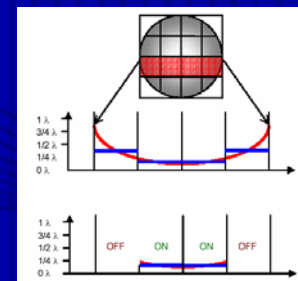
### Piston mirror:

- Phase of distorted wave-front is measured and averaged over a local area (single mirror size) of the wave-front
- Corresponding MMA mirror height (modulo  $2\pi$ ) is set to this average phase value → ‘flattened wavefront’

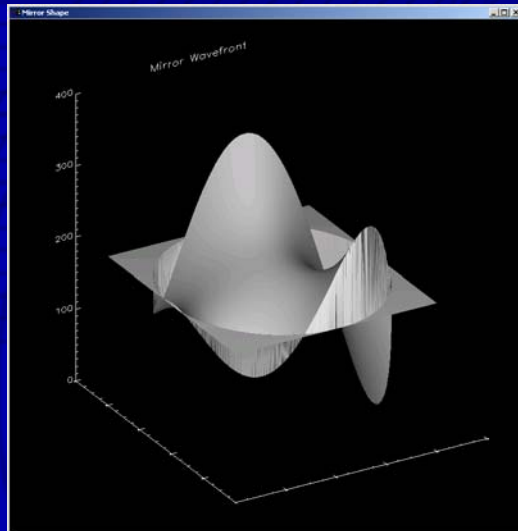


### Tilt mirror:

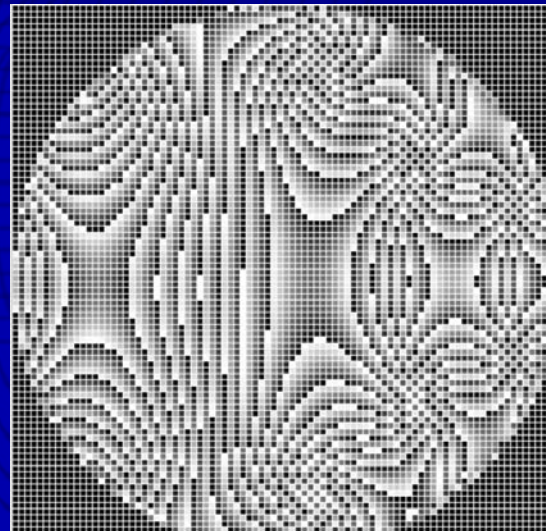
- Local phase measurement as for piston mirror
- Wave front sections which cause destructive interference are discarded → mirror is turned OFF



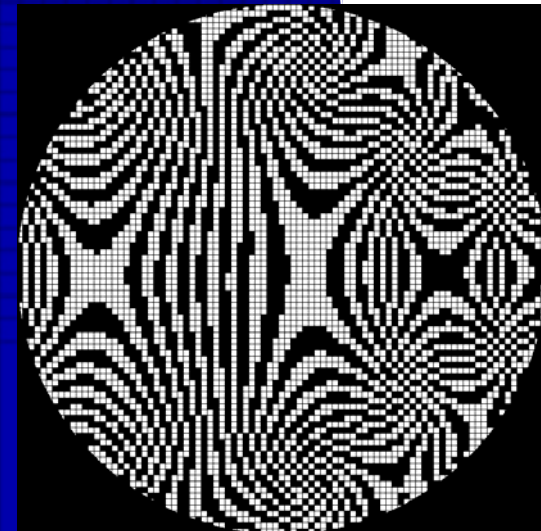
# Wavefront Correction with MMAs



Wavefront  
(height magnified)



Phase correction  
with Piston MMA  
(grey scale  
corresponds to  
height)



Phase correction  
with Tilt MMA  
(black = OFF,  
white = ON)

## FhG-IPMS MMA Technology

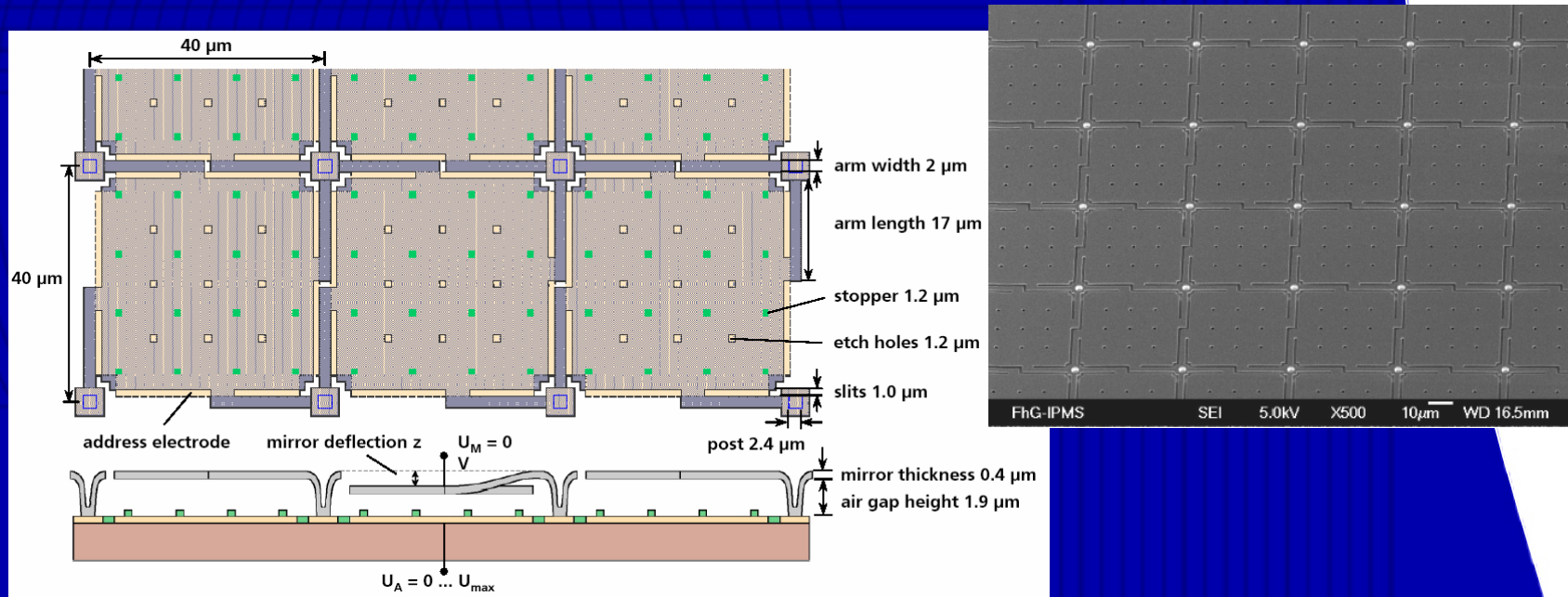
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- Fully monolithic integrated approach of micro-mirrors together with an underlying CMOS address circuitry (standard semiconductor fabrication technology)
- Active CMOS address matrix, like DRAM. One switching transistor and storage capacitor per matrix cell. Analog voltage levels define electrostatic deflection for each individual mirror element.
- CMOS process with 19 lithographic layers, address voltage capability up to 30V for larger mirror deflections.
- **Micro-mirrors are fabricated on top of the completed address circuitry within a fully CMOS-compatible process**
- Surface-micromachining requires three additional layers. Mirror elements, suspension arms and support posts are deposited with aluminium alloy.
- Ceramic pin grid arrays (PGA) package covered by an anti-reflective optical window.

# FhG-IPMS MMA Technology

## Piston MMA:

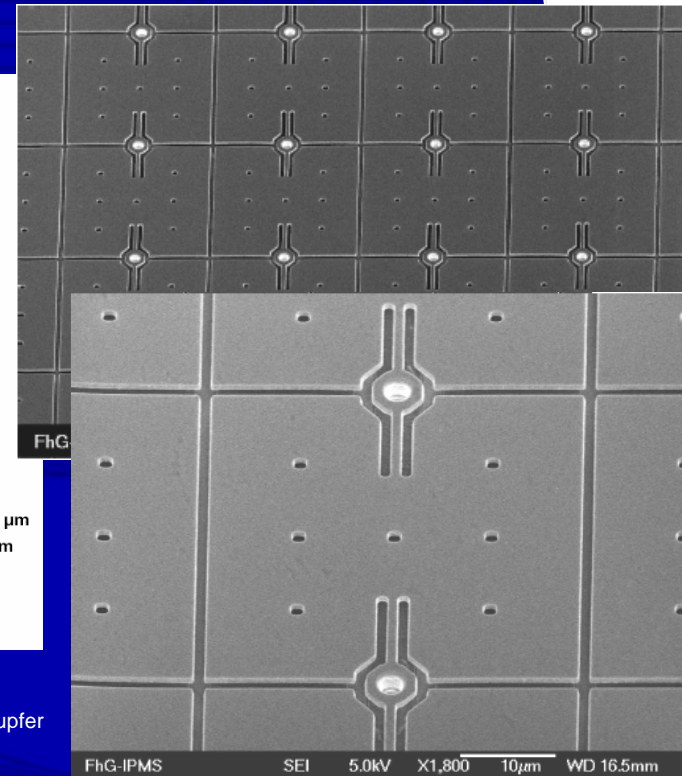
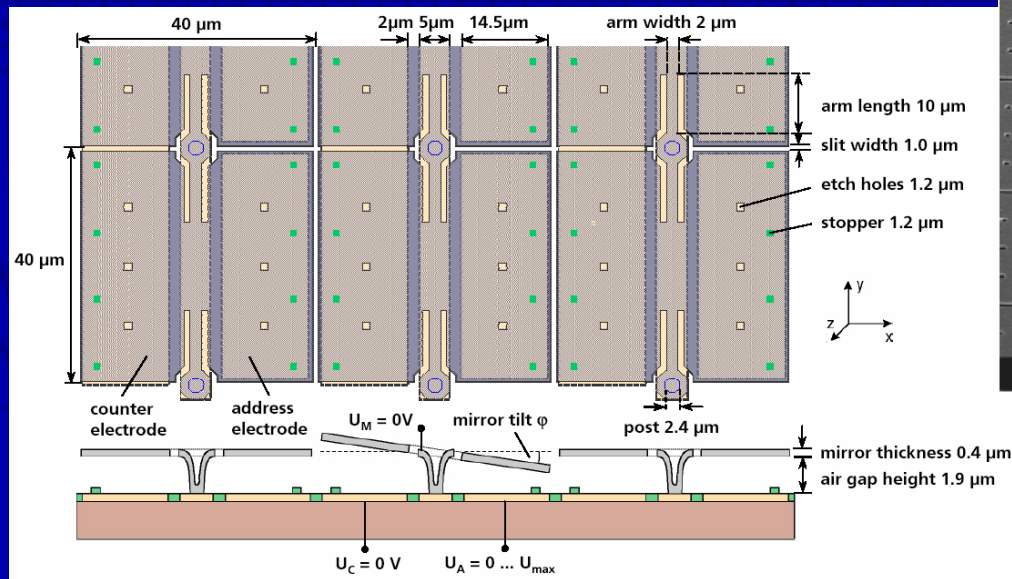
Square plate is suspended by four cantilever beams over an air gap with an underlying address electrode. Upon electrical activation the mirror plate can be continuously deflected in a piston-like motion as a function of applied voltage providing a continuous phase shift for each pixel.



# FhG-IPMS MMA Technology

## Tilt MMA:

Mirror plate is suspended by two torsional arms along the pixel center axis with the underlying address electrode extending only on one side, on the opposite side is a counter-electrode common to all pixels. Applying a voltage causes the mirror to rotate.



# FhG-IPMS MMA Technology

## Electronics and Software

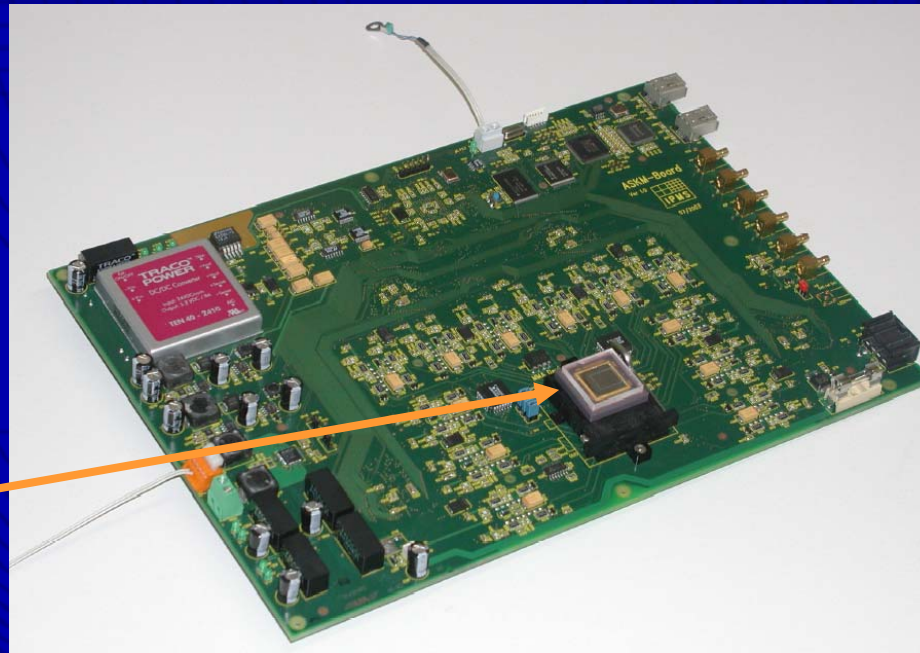
Bread-board based on traditional electronics with

- IEEE 1394 (FireWire) I/F
- ActiveX programming environment + Stand-alone GUI

Reprogramming rate

- 5 kHz maximum
- 50 Hz in Bread-board

MMA

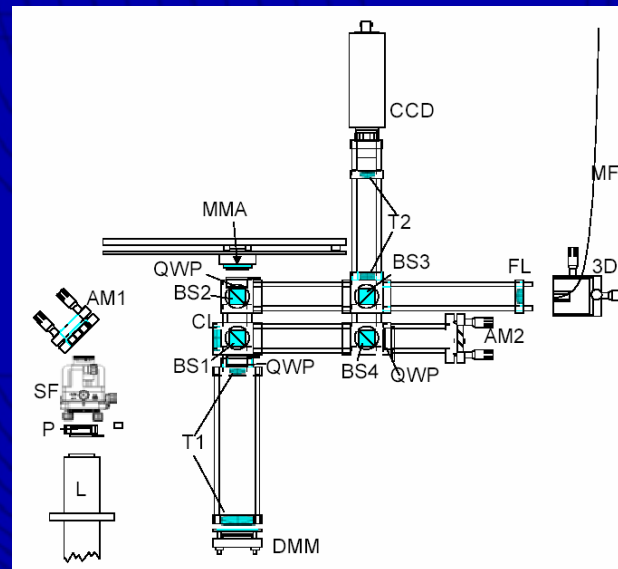


# Bread-board Tests

## Wave-front Correction Algorithms – 2 Methods

- Standard **wave-front sensing** (fast) with Interferometry Shack-Hartmann
- **Stochastic method** – (slow) does not require additional metrology!

Membrane Mirror (DMM) is used for Wave-front Generation



- 3DP: xyz positioner
- AM: adjustable mirrors
- BS: beam splitters
- CCD: camera chip
- CL: collimation lens
- DMM: deformable membrane mirror
- FL: focussing lens
- L: laser
- MMA: micro mirror array
- MF: monomode fibre
- P: polariser
- SF: spatial filter
- T: telescopes (with 2 lenses)
- QWP: quarter wave plates

# Results

## Tests with 4 types of wave-front distortions:

Wavefront denomination	Measured wavefront errors (CWFE1, CWFE2, CWFE3, SWFE)			
	CWFE1	CWFE2	CWFE3	SWFE
Measurement with piston MMA (continuous)				
WFE (rms)	0.13 $\lambda$	0.25 $\lambda$	2.0 $\lambda$	0.17mm cover plate edges
WFE (PV)	0.7 $\lambda$	1.2 $\lambda$	7.9 $\lambda$	plate edges
Measurement with flip MMA (binary)				
<b>Achieved coupling efficiency with piston MMA</b>				
With correction	63%	49%	40%	42%
Without correction	51%	1.4%	0.27%	8.1%
<b>Achieved coupling efficiency with flip MMA</b>				
With correction	35%	8.1%	4.2%	7.9%
Without correction	34%	4%	0.15%	1.0%

**Max. coupling efficiency: Piston MMA = 65.5% Tilt MMA = 40.5%**



## Conclusion

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Both MMA devices can be used for wave-front correction in an Adaptive Optics System.

Tilt mirror has low efficiency and the performance is strongly wave-front error depended

Preferred Choice: **Piston MMA**

- delivers the heighest Coupling Efficiency
- corrects wave-front errors with high spatial frequency and even discontinuities.
- corrects 'flat' wave-front errors due to it's high resolution (2 nm)