



The study of MEMS failure mechanisms and Reliability / Qualification testing methods

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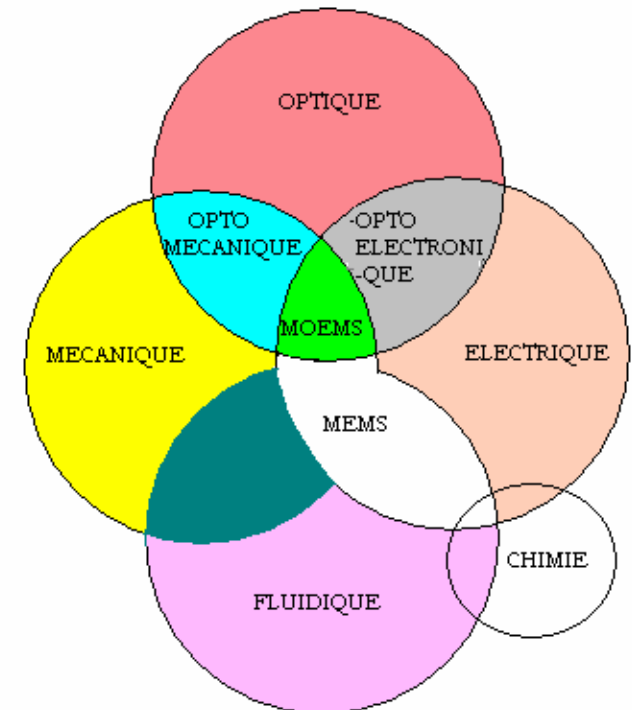


Content

- Overall project overview
- Presentation of the ESA/CNES Physical Analysis
- Presentation of the test plan
- Presentation of the test results
- Presentation of CNES FailureAnalysis
- Conclusion of the activity

1. Aim of the study

- **To understand the issue related to MEMS**
Assess MEMS based Gyro Reliability
Define the tight experiments and testing
- **MEMS (MicroElectroMechanicalSystems) :**
10 μ m size intelligent systems
- **Miniaturisation of platform electronics by the use of MEMS**
Interest for CNES, ESA and ASTRIUM
- **MEMS overview : applications in space, MEMS technology, failure mechanisms, MEMS reliability test methods.**
- **Elaborate testing of MEMS : the micro-gyroscope**
- **Guideline redaction for the evaluation of MEMS**





MEMS: Interest for space

Launch cost

**Mass
production
methods**

**Weight
reduction**

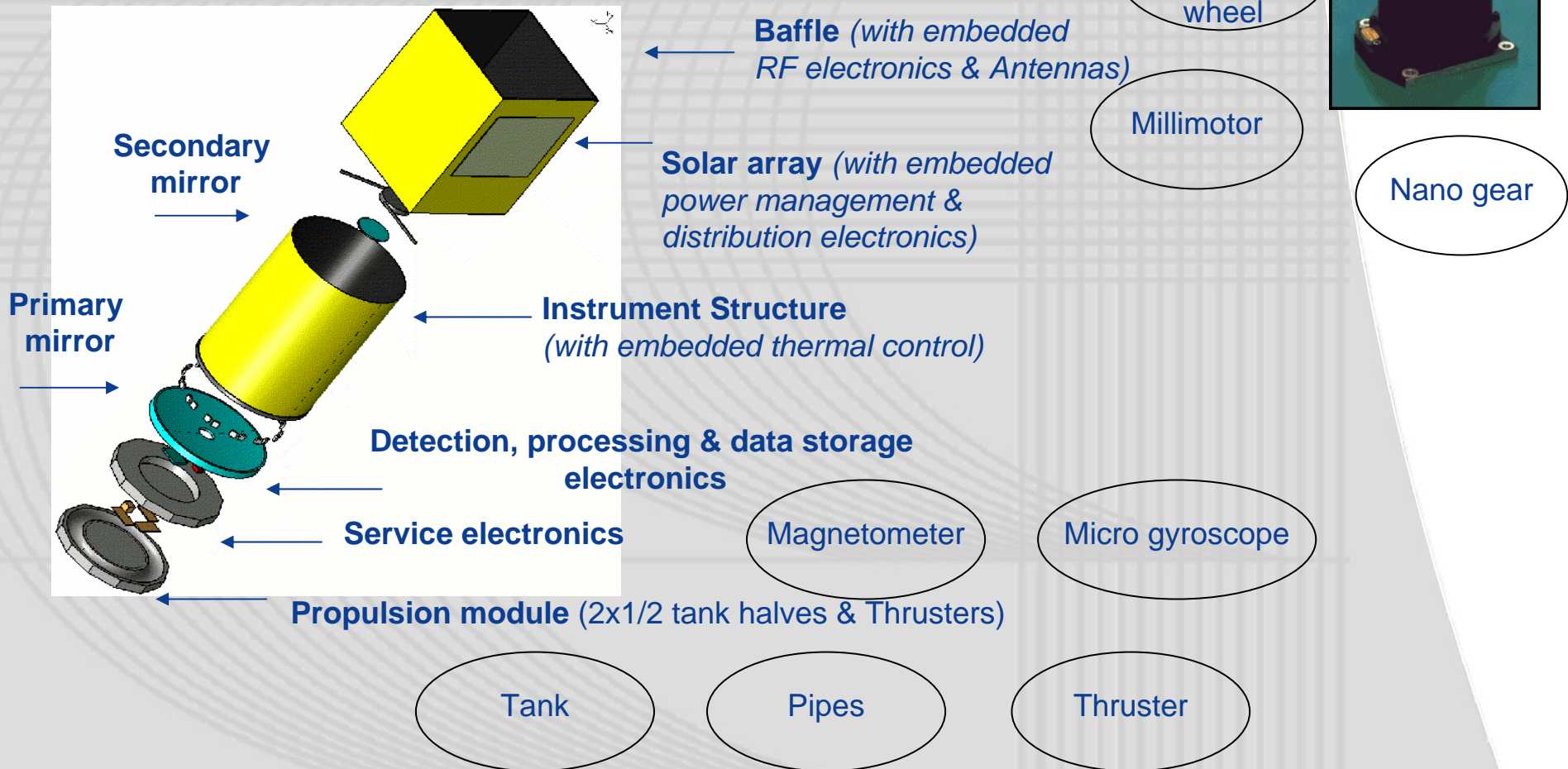
**Low power
consumption**

**Satellite
miniaturisation**

Easy manipulation



Which micro-devices in a satellite?





Possible space applications for MEMS

➤ The space industry is not a major player in the MST field but a “fast follower”.

TODAY (not in space)

Pressure sensors

Airbag accelerometers

Printers

Read/Write heads for hard
disk drives

FUTURE (in space)

Micro gyroscopes and
magnetometer (in AOCS)

Optical instrumentation

RF components

Power supply

Cooling system

Optical payloads

**MEAN
TERM**

**LONG
TERM**



Gyroscopes: Sensor used to detect inertial angular motion.

- *Mechanical gyros*

RIG (Rate Integrating Gyro) now replaced by
DTG (Dynamically Tuned Gyro) ↘

Eurostar 2000

Eurostar 2000+/3000 - ATV -
Spot5 / Helios2 / Metop

- *Optical gyros*

RLG (Ring Laser Gyro) →
FOG (Fibre Optic Gyro) ↗

Ariane – Rosetta / Mars express

Will replace current techno. On new
developed S/C (Pleiades, Aeolus,
Astrobus,...)

- *Resonant gyros*

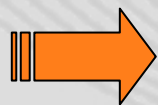
HRG (Hemispherical Resonant Gyro) →
μVSG (Vibrating Silicon Gyro) ↗

Rocsat, Kompsat
(Micro satellite)



Gyroscopes performances status

	<i>Bias stability</i>	<i>Angle Random Walk</i>	<i>Scale factor</i>
	RF	ARW	SF
<i>Mechanical gyros</i>			
RIG/DTG	0,1°/h → 0,001°/h	0,1°/√h → 0,001°/√h	1000 ppm
<i>Optical gyros</i>			
RLG	1°/h → 0,01°/h	0,1°/√h → 0,01°/√h	10 → 1 ppm
FOG	10°/h → 0,001°/h	0,01°/√h → 0,0001°/√h	1000 → 20 ppm
<i>Resonant gyros</i>			
HRG	10°/h → 0,001°/h	0,01°/√h → 0,0001°/√h	200 → 50 ppm
VSG	0.1°/s → 5°/h	1°/√h → 0,1°/√h	1% → 1000 ppm



The accuracy and bias stability of μ -gyros do not yet meet the requirements of satellite inertial systems.



SiRSS: Vibrating Structure Gyroscope (BAe)

Solid state sensor based on the coriolis effect.

Single axis sensing element (less than one centimetre in diameter) and electronics in the same package (135g in weight).

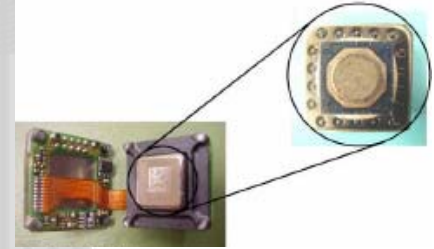


Performance : **Scale factor variation..... within +3% to – 3%**
Zero bias.....+2°/sec to –2°/sec
Axis alignment.....+/- 0.5°

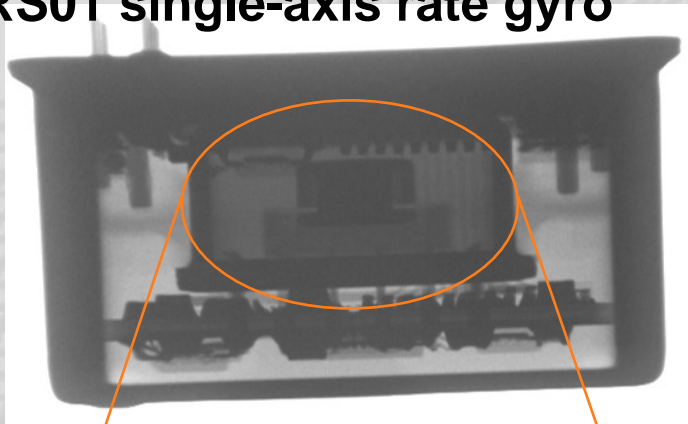
Performance tests over temperature:
(- 40°C / + 70°C)

Output noise
Bias
Scale Factor Variation
Axis alignment





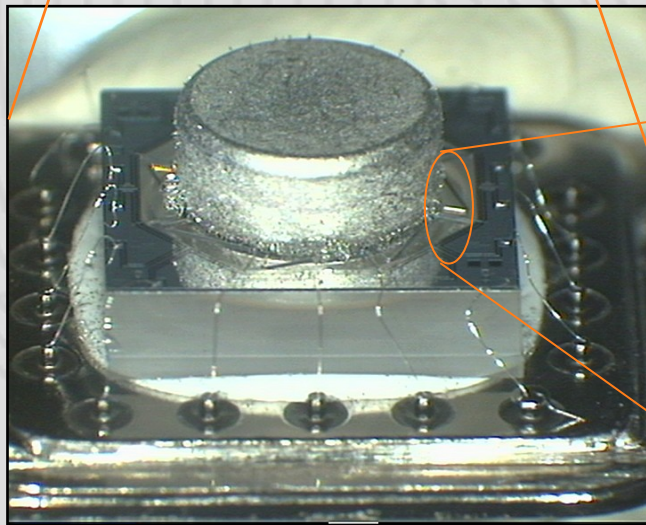
SiRRS01 single-axis rate gyro



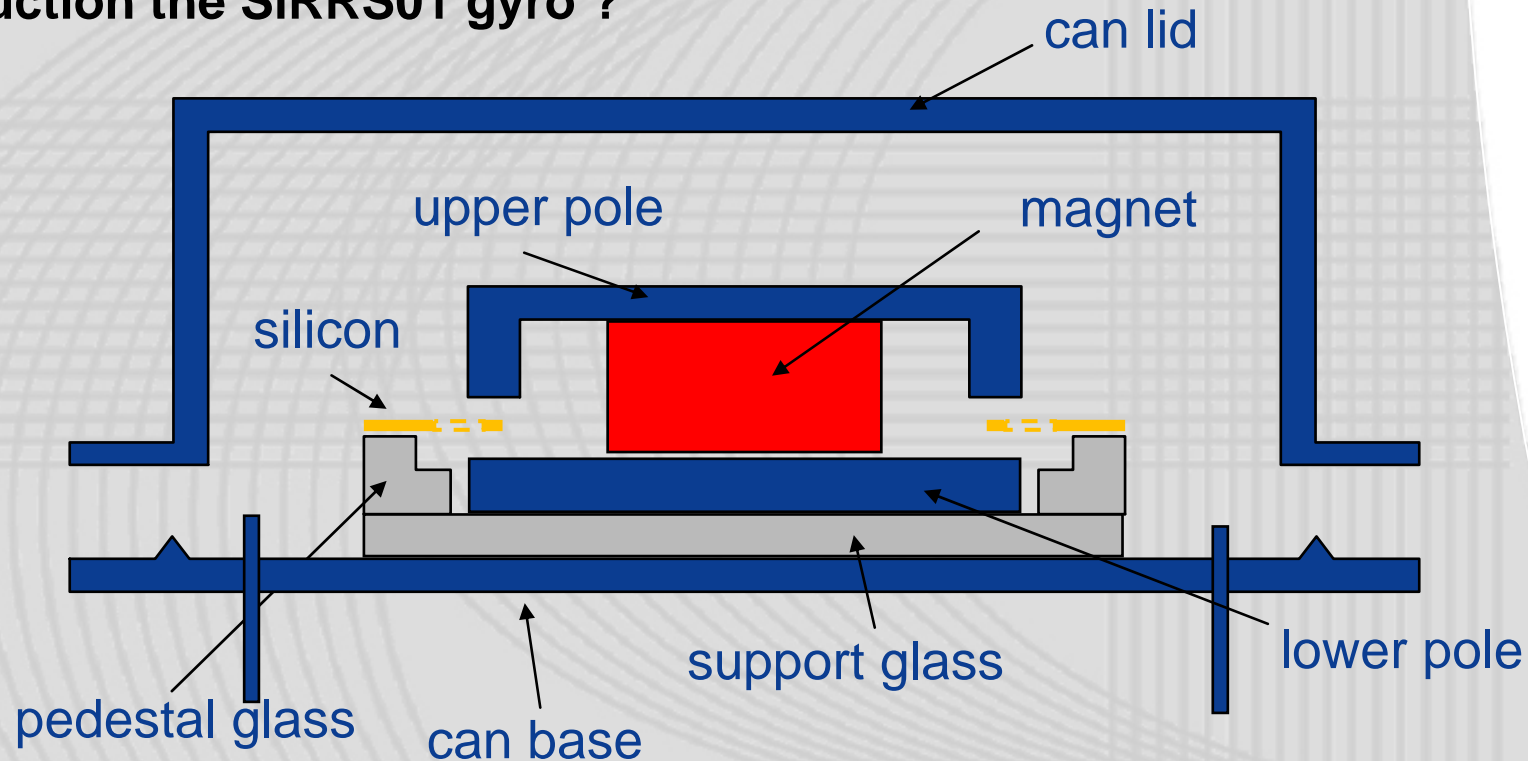
✓ Gyro made of a mechanical part, the 'sensor head', and an ASIC to put the gyro into vibration, control the vibration and measure the rate of turn.

✓ Vibrating Structure Gyro based on the coriolis effect.

✓ 'Deep trench etching' process enabling the production of the tiny micro-machined silicon ring.



Construction the SiRRS01 gyro ?

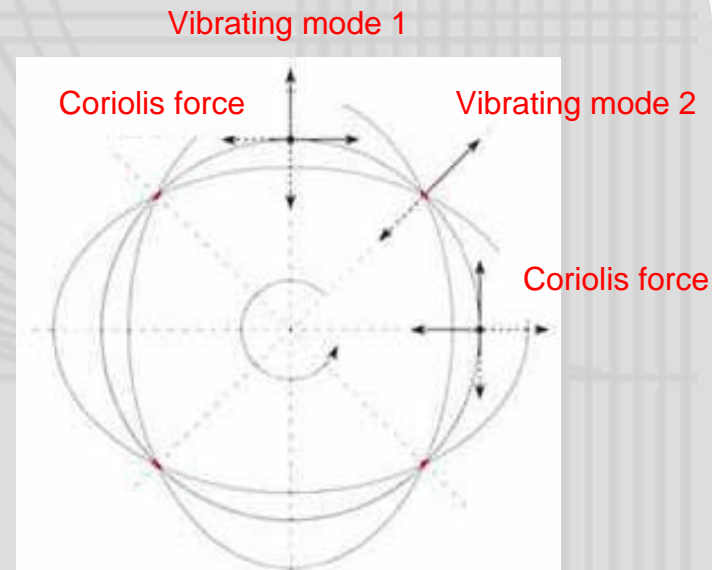
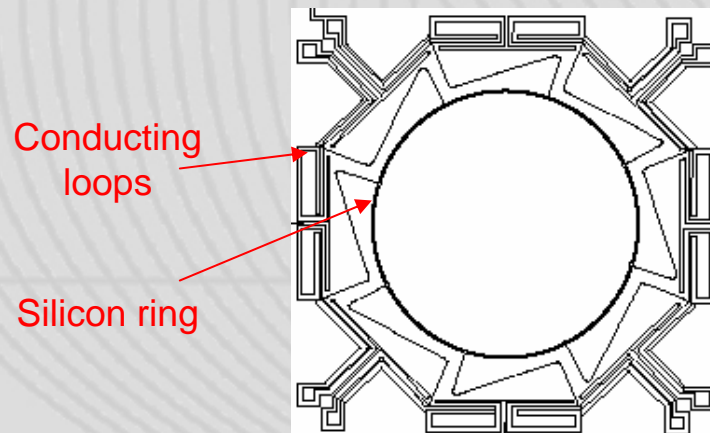
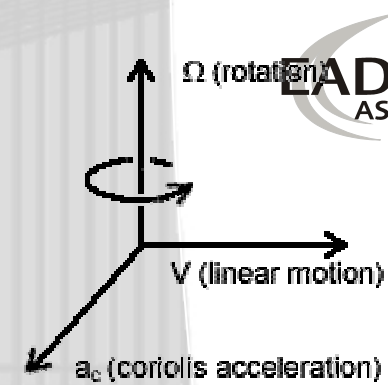


- ✓ Bulk micro-machining technology: silicon etched to create the sensor ring
- ✓ Silicon-on-insulator (SOI) substrate: silicon anodically bonded to a glass support



Functioning principles of the SiRRS01 gyro?

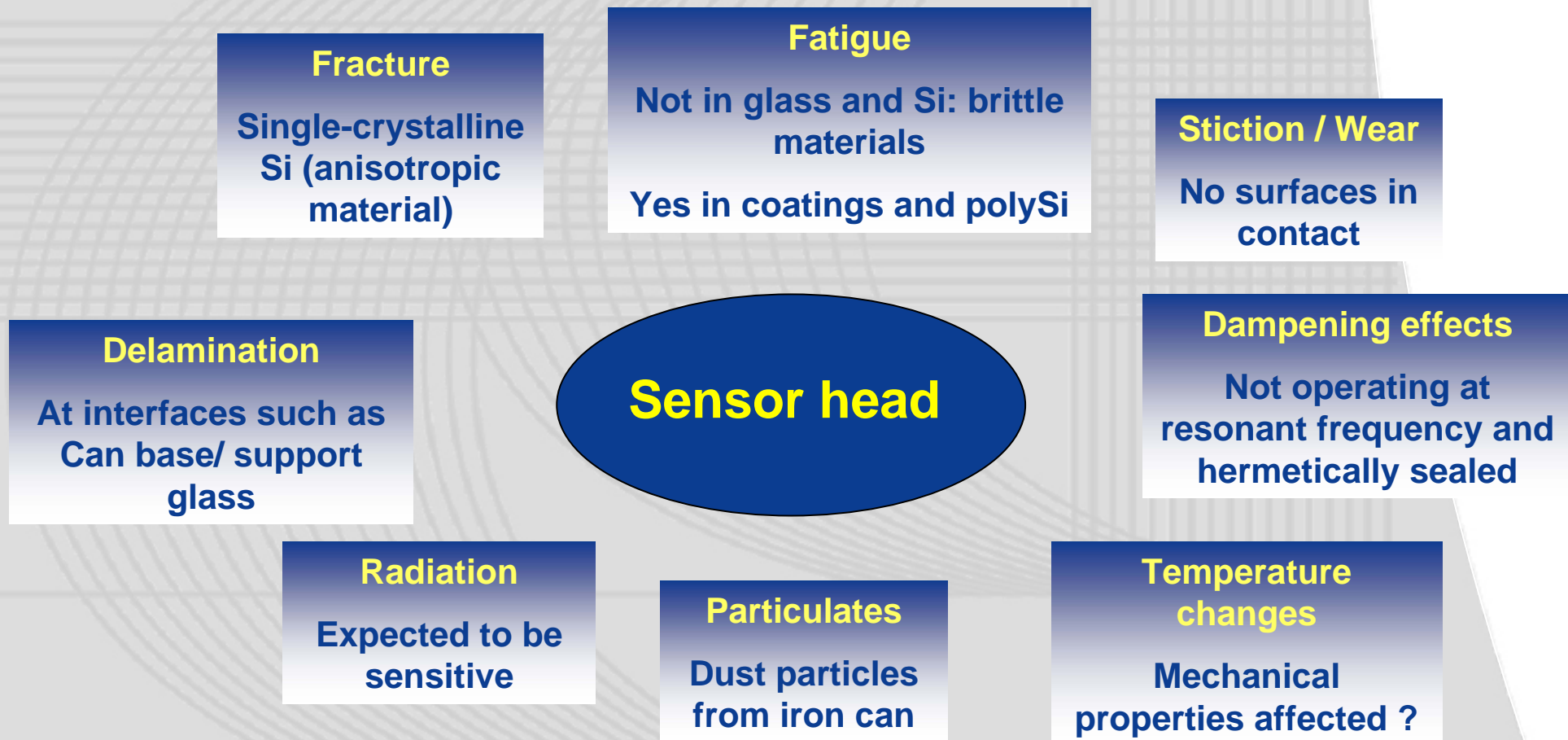
- ✓ Based on the Coriolis Effect: Coriolis acceleration experienced by a particle undergoing linear motion in a rotating frame of reference.
- ✓ Resulting acceleration directly proportional to the rate of turn.
- ✓ Vibratory motion coupled from a primary vibrating mode into a second mode when sensor experiencing angular rate.





Potential failure mechanisms of the SiRRS01 gyro

Focus made on the sensor head : {silicon ring / metallic resonator / glass bonded}



Potential weaknesses also assessed by [ESA/CNES Constructional Analyses](#)



Failure mechanisms vs testing

- SiRRS01 silicon rate sensor more sensitive to fracture and delamination.
- **Thermo-mechanical** tests and even life-test may evidence these failure mechanisms.
 - Shocks and temperature testing may induce fracture and delamination
 - Shocks could lead to early end of life of the structure, as vibrations do by inducing distortions or bending of the structure.
 - Symmetry of the ring design offer excellent rejection of linear vibration.
- Electronics in a closed loop around the sensing part and may prevent the system from reaching its functional limits even under harsh conditions.
 - Radiation testing will be performed separately on the sensor head alone (but previous testing at ESA demonstrated MEMS gyroscope (sensor and electronic sensitivity to TID))

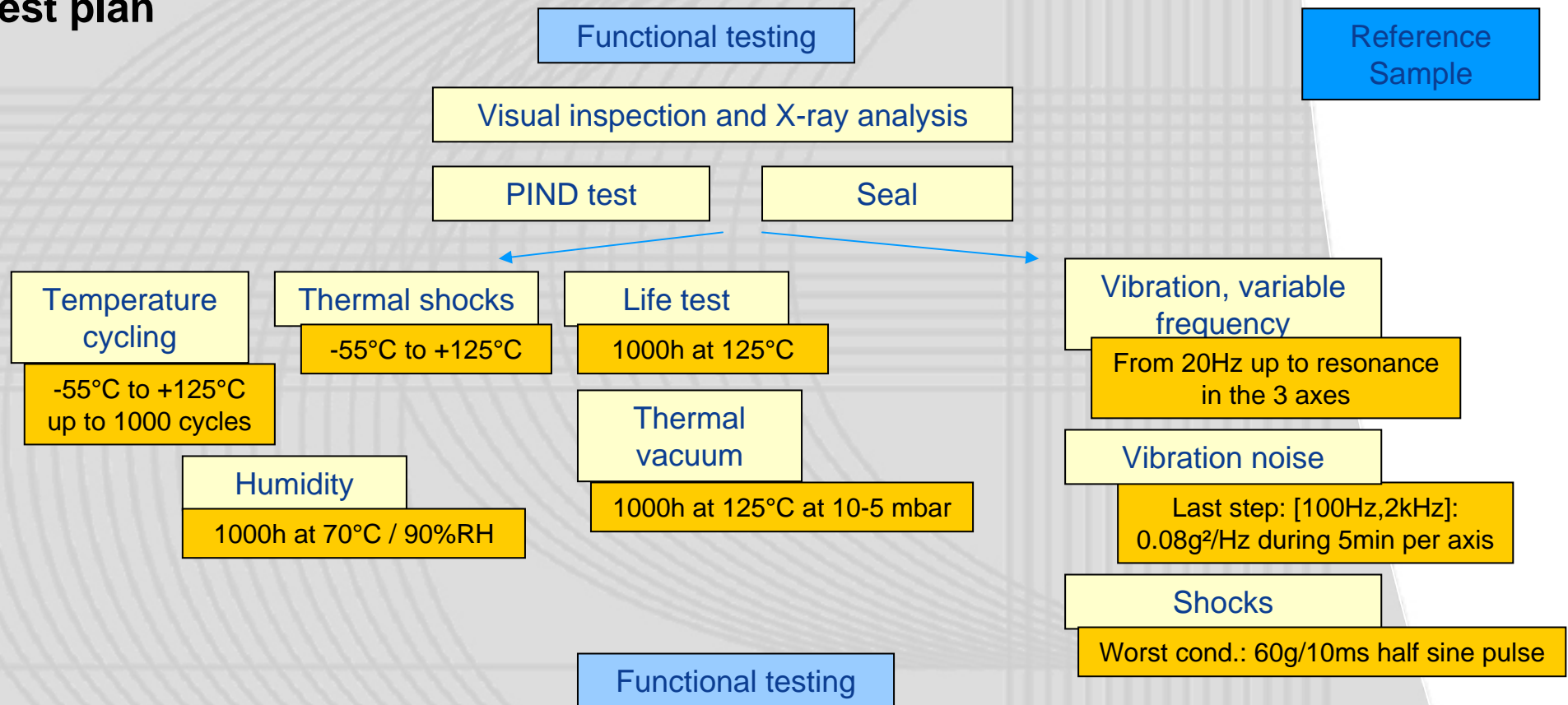


Performance and reliability testing

Operating temperature	- 40°C to + 75°C
Humidity	100% RH
Vibration (operational)	10g rms [20Hz to 2KHz]
Shock (operational)	60g (30ms, 1/2 sine)

- No space testing specification at equipment level for angular rate sensors.
- Procedure of reliability testing based on microcircuits specification : MIL-STD-883E 'Test Method Standard, Microcircuits'
- Test conditions defined with the SiRRS01 rate sensor specification and published data on other type of MEMS.
- Mechanical shocks performed on a sample up to destruction.
- Failure Analysis to be performed in case of anomalous parameter measurements or destructive events.
- Limited number (7) of gyros including a sample of reference to perform reliability testing.
- Sensor and electronics kept together in the same package during tests.

Test plan



- ❑ Basic performances (Bias / Bias repeatability / Noise) to be performed between each tests.
- ❑ 3 gyros will undergo temperature testing while 3 others mechanical testing.

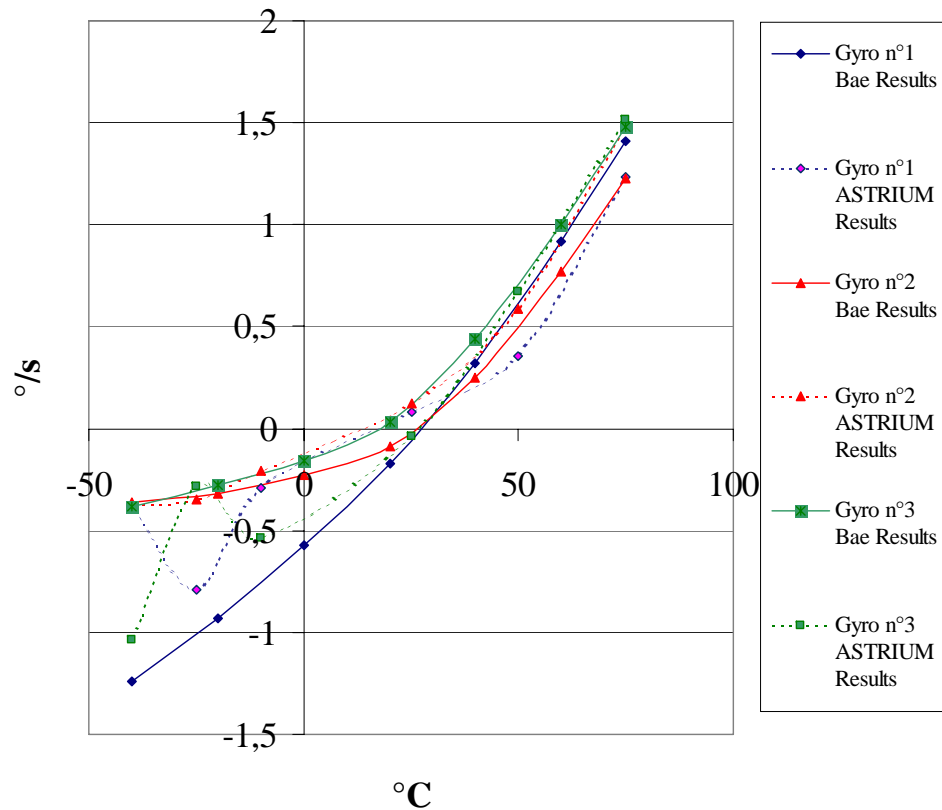


Test sequence per part

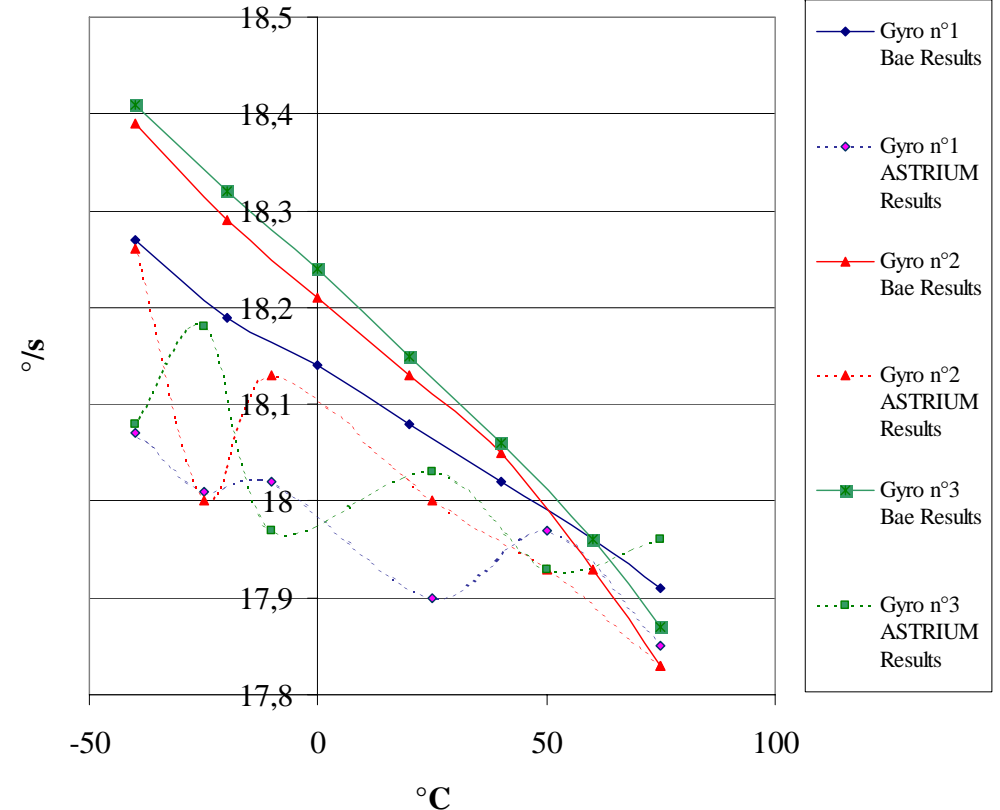
S/N	
10805	1000 thermal cycles + life test (1000 h@+125°C)
10880	Technical hitch [too high temperature seen by the component] → PIND test
10882	Life test+ thermal vacuum + life test
20580	Mechanical test : vibrations and shocks
20582	Mechanical test : vibrations and shocks
20592	Mechanical test : vibrations and shocks
20760	ESA destructive DPA
20762	ESA reference part. (S/N ESA)
21048	1000 thermal cycles + life test (1000 h@+125°C)
21050	Technical hitch [wrong polarization] → PIND test

Functional testing: Astrium initial measurements

Bias : Comparison with BAe data



Scale Factor : Comparison with BAe data



Gyros show a rather stable behaviour over temperature



INITIAL TEST RESULTS : Comparison with BAE results: Main differences

- NOISE

Measured (ASTRIUM & CNES) : $> 0.7 \text{ }^\circ/\sqrt{h}$

SiRSS datasheet : $< 0.2 \text{ }^\circ/\sqrt{h}$

Difference not understood. Measurement method?

- DRIFT STABILITY

Two family of gyros !

1st LOT : rather stable typ. $\pm 50^\circ/h$

(data sheet : $< 2 \text{ }^\circ/h$!!)

2nd LOT : very unstable

(up to $1500 \text{ }^\circ/h$ per day)

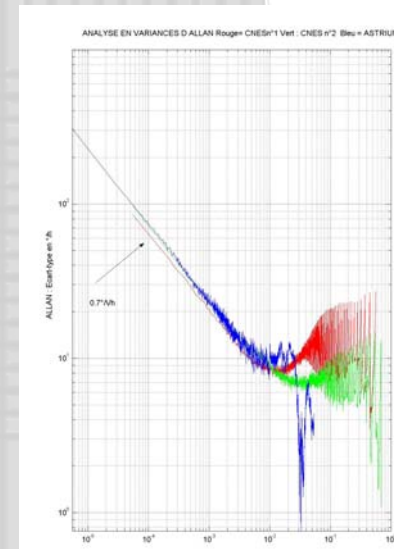
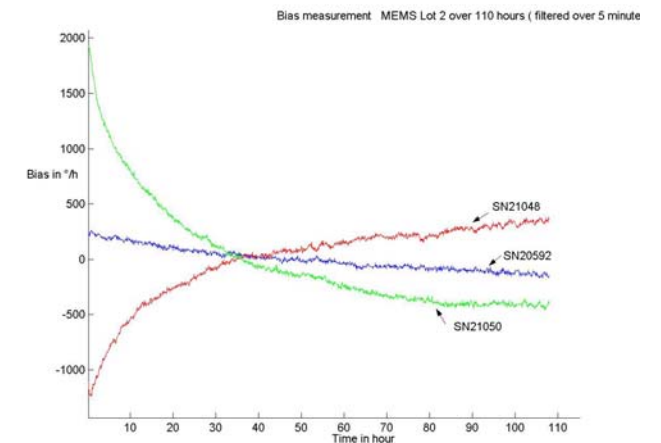
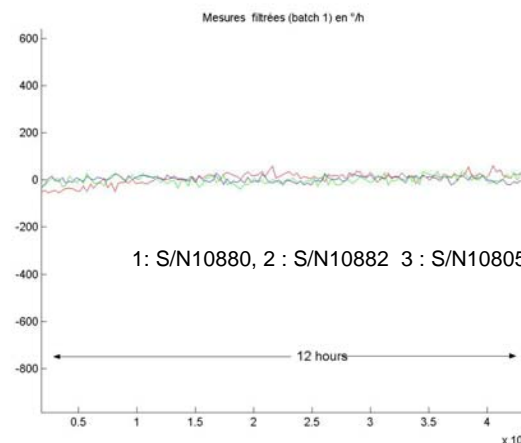
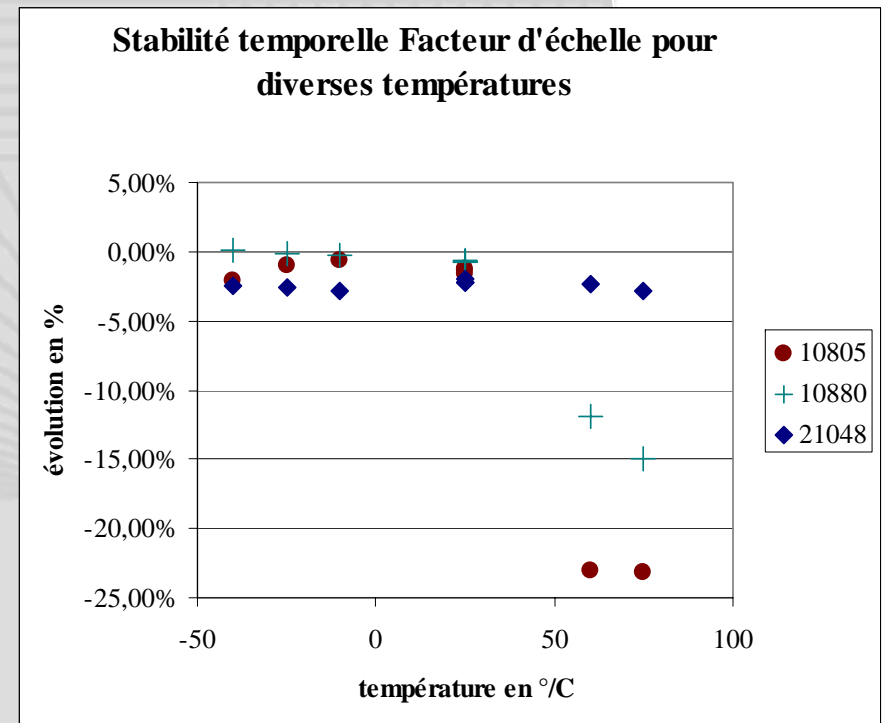
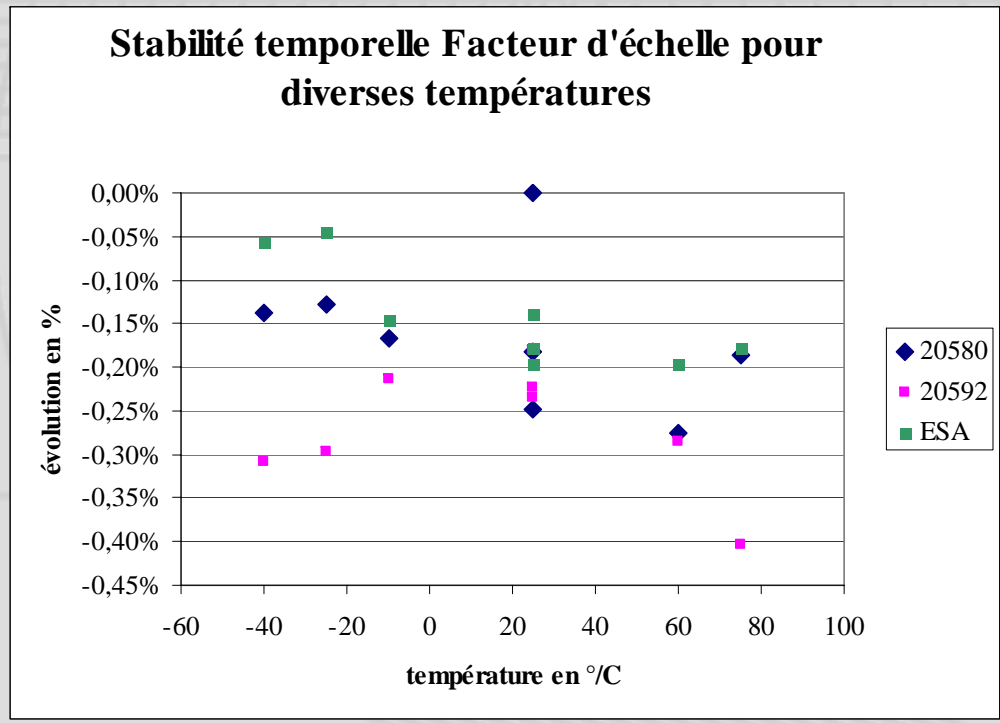


Figure : comparison between ASTRIUM and CNES VA measurements



Test Results: SCALE FACTOR STABILITY OVER TIME

- Data sheet BAe :**
 - OK : n° 20580, n° 20592, n° ESA
 - NOT OK : n° 10805, n° 10880, n° 21048
- Nominal : 18.2 mV/°s**
- Repeatability : +/-1% (1 sigma)**





Test Results: SCALE FACTOR LINEARITY

- Data sheet BAe :

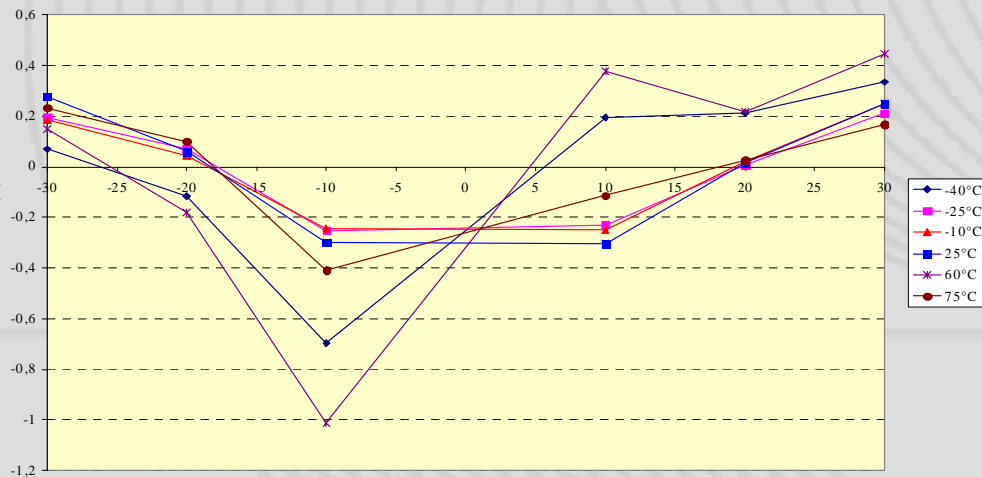
Linearity +/-1% of full scale

OK : n° 20580, n° 20592, n° ESA

NOK : n° 10805, n° 10880, n° 21048

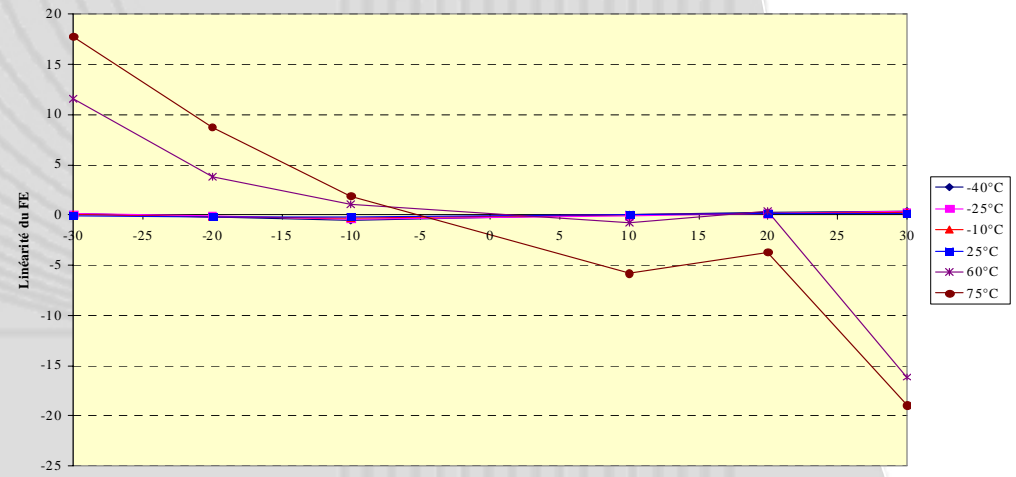
		20580	20592	21048	ESA	10805	10880
Final	Facteur d'échelle linéarité (max)	+/-0,4%	+/-0,5%	+/-4%	+/-1%	+/-15%	+/-20%

Linéarité du facteur d'échelle



Vitesse de rotation (°/s)
N° ESA

Linéarité du facteur d'échelle



Vitesse de rotation (°/s)
N° 10880

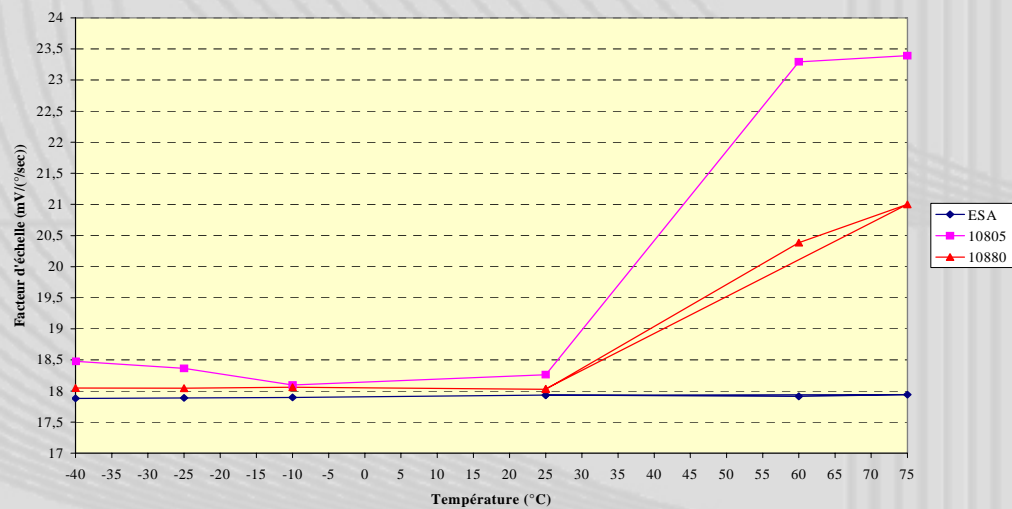


Test Results: SCALE FACTOR SENSITIVITY TO TEMPERATURE

- Data sheet BAe : OK : n° 20580, n° 20592, n° ESA
Variation with temperature : +/-3% NOK : n° 10805, n° 10880, (n° 21048)

	20580	20592	21048	ESA	10805	10880
Facteur d'échelle en température Stabilité (max-min)	0,58%	1,37%	2,37%	0,35%	28,89%	16,52%

Evolution du facteur d'échelle en fonction de la Température



Test Results: BIAS STABILITY OVER TIME

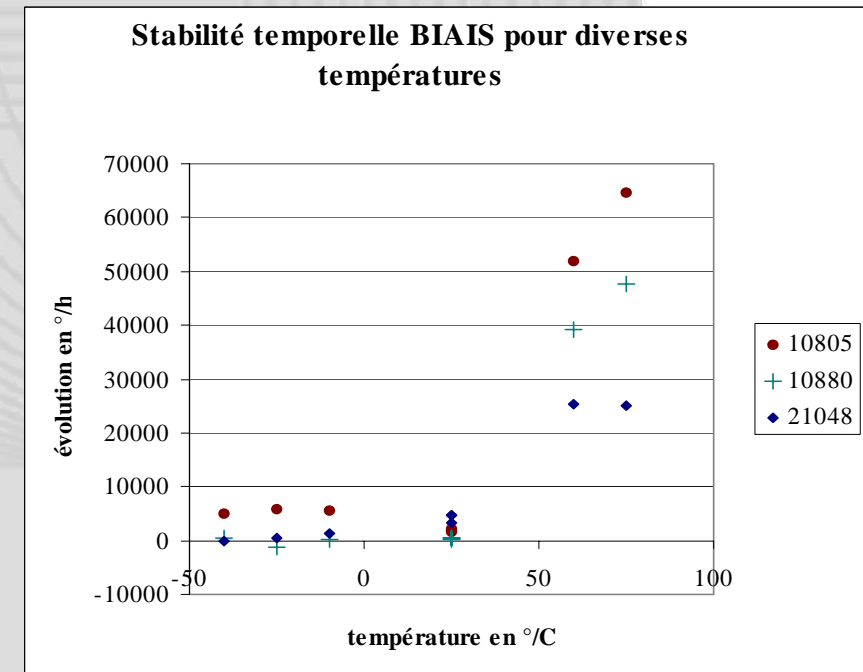
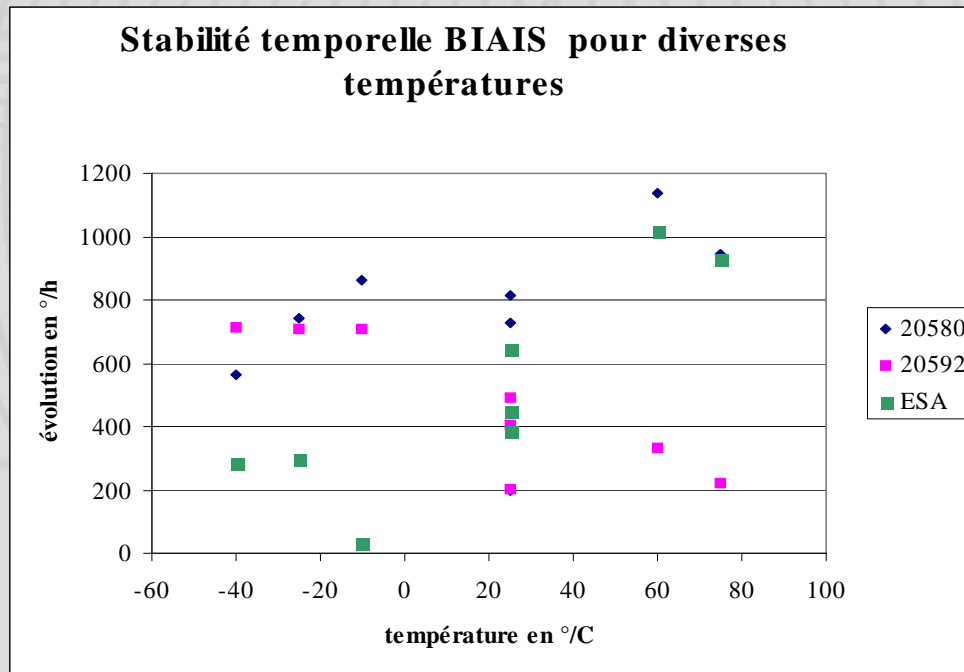
- Data sheet BAe :

Setting @20°C) : +/- 0.3°/s

Repeatability : 0.1°/s = 360 °/h (1 sigma)

OK : n° 20580, n° 20592, n° ESA

NOK : n° 10805, n° 10880, n° 21048



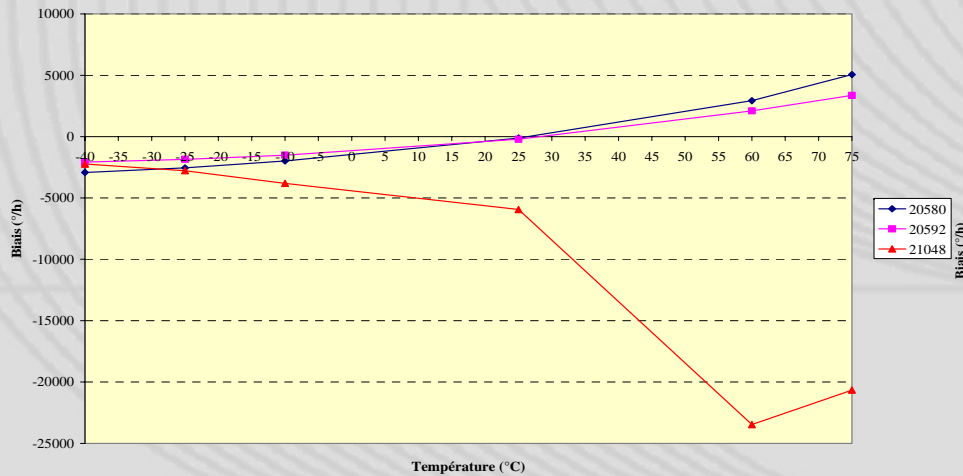


Test Results: BIAS SENSITIVITY TO TEMPERATURE

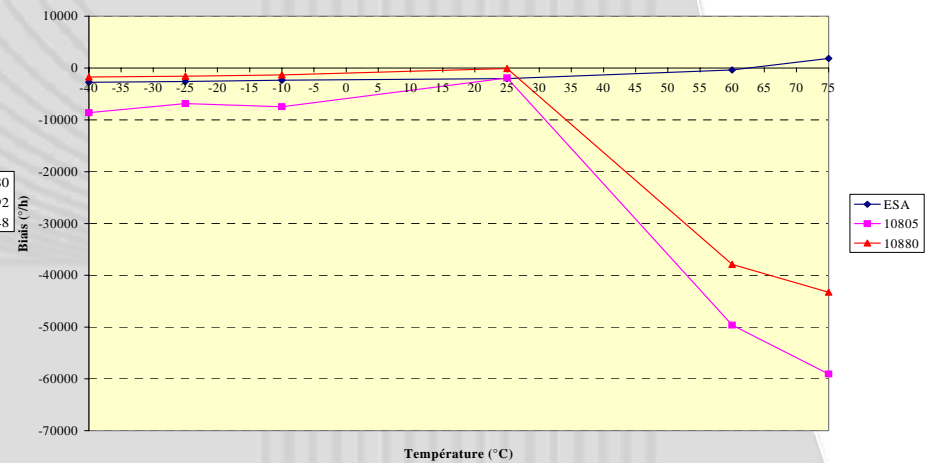
- Data sheet BAe : ≈OK : n° 20580, n° 20592, n° ESA
 Variation with temperature : $\pm 0.2^\circ/s$ NOK : n° 10805, n° 10880, (n° 21048)
 (or $720^\circ/h$)

	20580	20592	21048	ESA	10805	10880
Biais en température Stabilité (max-min) en $^\circ/h$	7975	5442	21234	4616	57422	43276

Evolution du BIAIS en fonction de la Température



Evolution du BIAIS en fonction de la Température





DRIFT STABILITY OVER 1 HOUR

- Data sheet BAe :
Stability : 3°/h

Drift stability over 1 hour , in °/h						
	20580	20592	21048	ESA	10805	10880
25°C initial	-214	-325	-6340	-2508	-2353	-244
25°C final	87	-164	-9342	-2226	-1715	-31
Stability over 1 hour	301	161	-3001	282	638	213

NOISE

- Data sheet BAe :

≈OK : n° 20580, n° 20592, n° ESA,
NOK : n° 10805, n° 10880 , n° 21048

ARW : 0.2°/√h

ARW , in °/√h						
	20580	20592	21048	ESA	10805	10880
25°C initial	0,75	0,75	0,83	0,7	1,44	1,44
25°C final	0,75	0,75	0,83	0,7	1,29	1,39

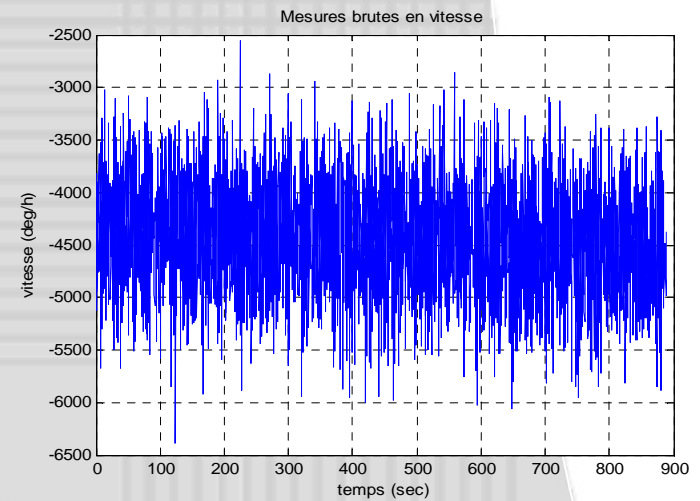
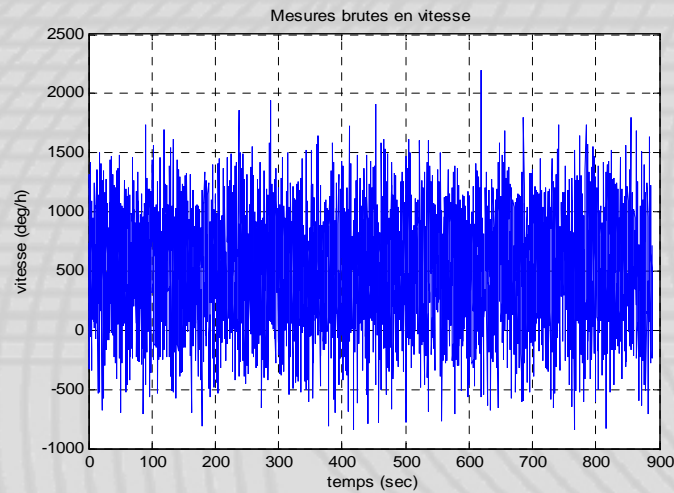


NOISE

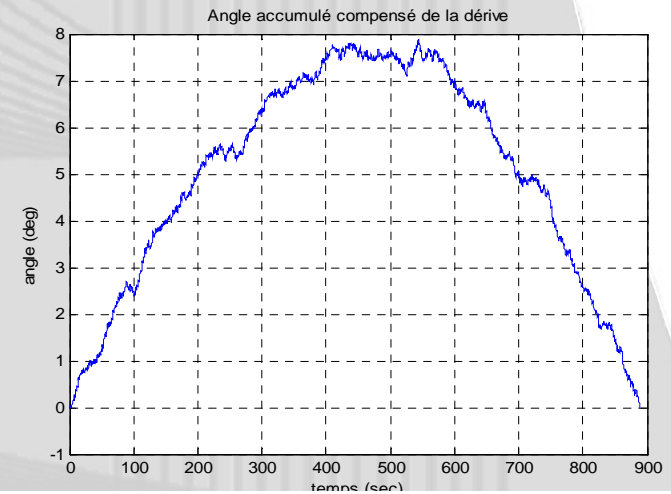
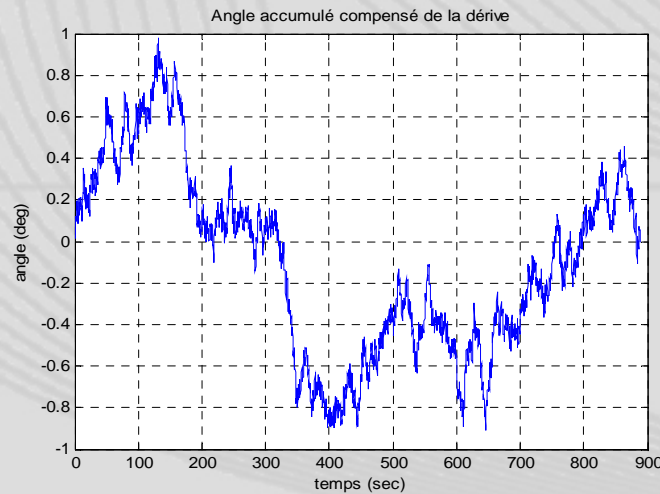
N°20580 : ~OK

N°21048 gyro : NOK

Vitesses



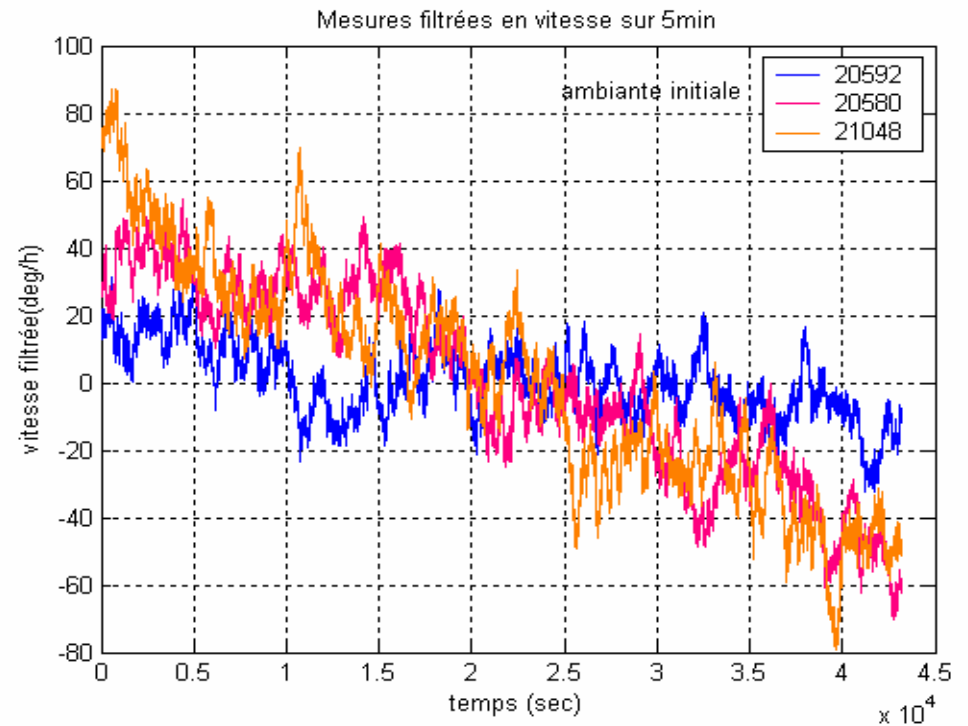
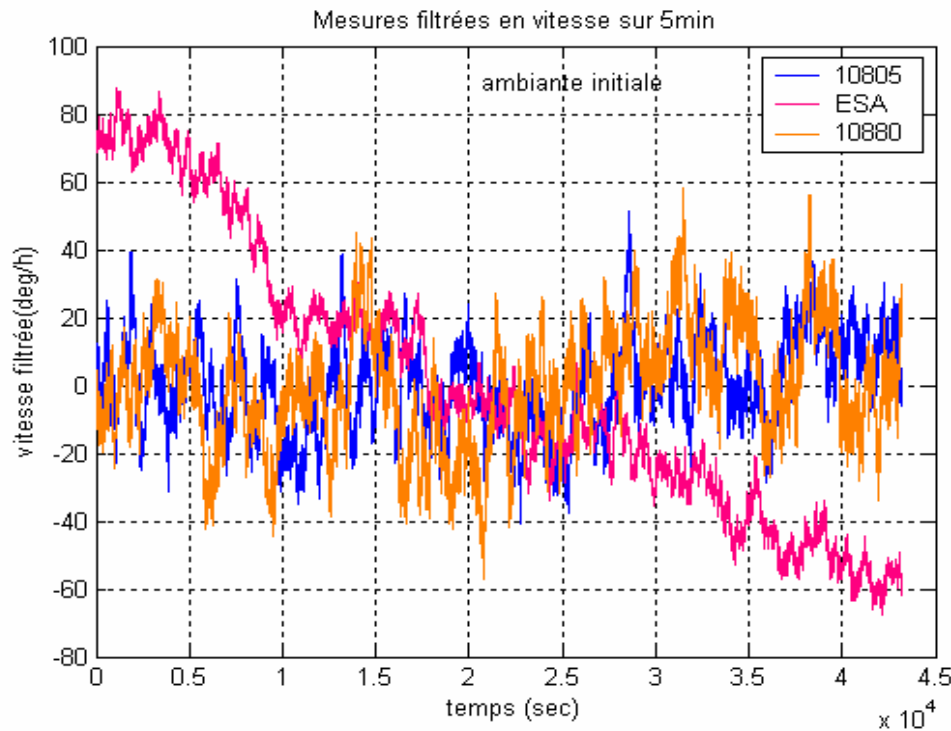
Angles





Filtered (5 min) outputs versus time

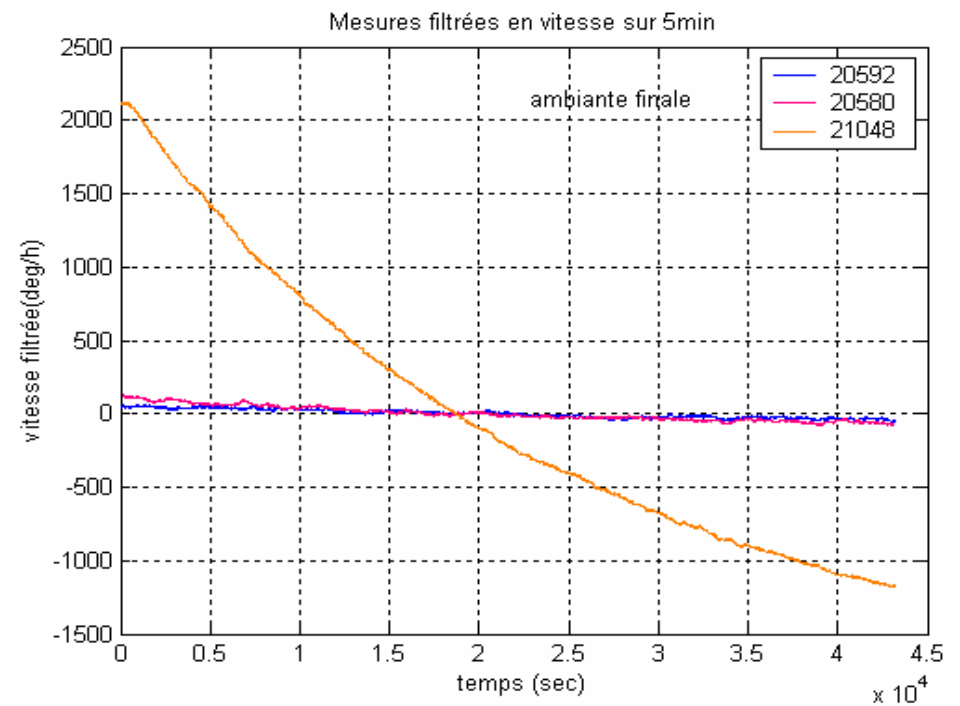
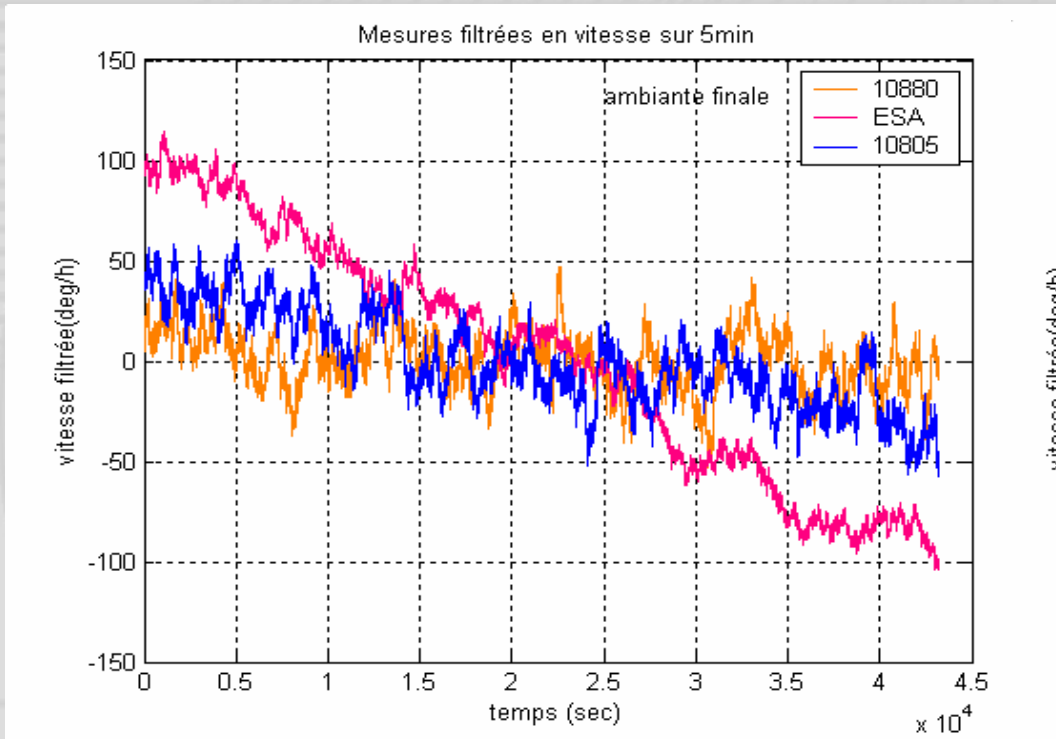
Rate variation wrt mean value



Initial tests @25°C (over 12 hours)

Filtered (5 min) outputs versus time

Rate variation wrt mean value



Final tests @25°C (over 12 hours)

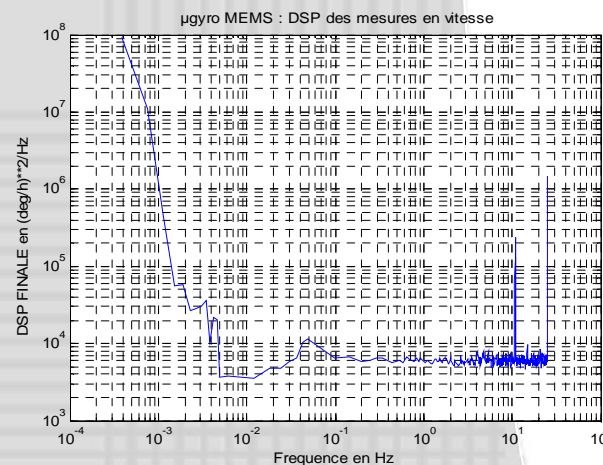
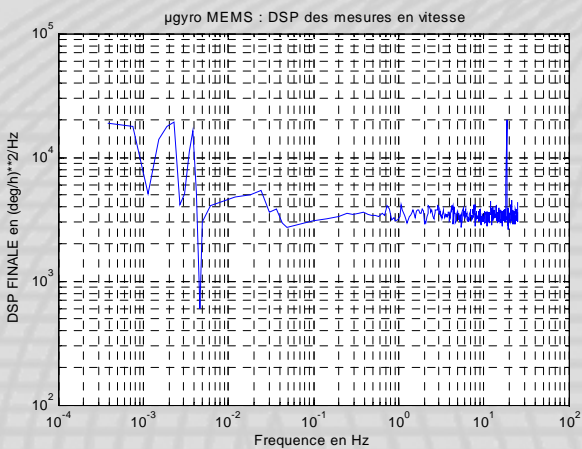


NOISE

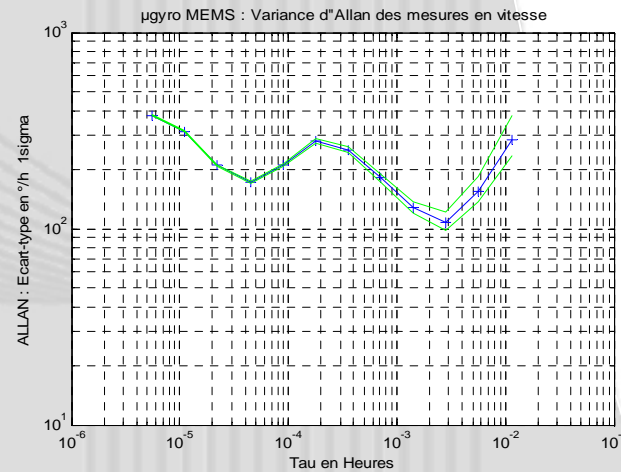
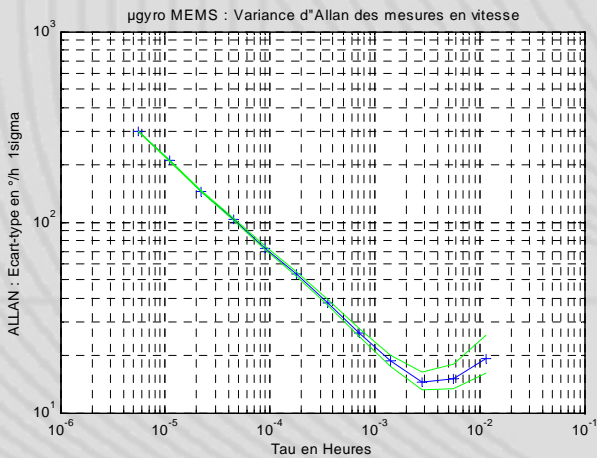
ESA gyro : OK

N°21048 gyro : NOK

DSP



Allan Variances





Test results summary

- **Initial Measurements:**
2 populations of gyro could be identified
- **Mechanical environments (vibrations and shocks):**
Good survivability
Rather low impacts on performances
- **Thermal environments/thermal cycling (very severe : -55°C , +125°C) & life test @125°C:**
Important impacts on performance (at completion of testing, all gyroscopes exhibited erratic behaviour on drift)
Failures observed



CONCLUSION

Findings:

- large disparity of the SiRSS in terms of performances, seems to be related to gyroscope disparity in terms of manufacturing (observed during Failure Analyses and additional X-Ray inspection @ Astrium); evolution of electronic design and COTS used observed
- degradation of performances was observed: erratic behaviour far above expectation (one or two order of magnitude) but difficult to associate this behaviour to MEMS or its electronics.

Follow-on discussion:

- first contacts with BAe confirmed a first set of measurements made by Astrium and acknowledged that disparity may be associated to changes in the fabrication process (use of different metallisation scheme)
- Crack identified during Failure Analysis confirmed by BAe as a possible cause of degradation (change of mechanical properties of the MEMS sensor)

Way Forward:

- New ESA activity starting with the Gyroscope Manufacturer:



**Thanks to ESA ESTEC and CNES for
their cooperation in this study**