

Plated Through Reliability and Material Integrity Results for 24 Materials Processed Through Lead Free Assembly

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5th EMPPS Workshop

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Agenda

- Introduction
- Test Vehicle, Test Protocol & Reflow Conditions
- Capacitance Testing Protocol Overview
- Results of Material Robustness in Pb-Free Assembly
- IST Testing Protocol Overview
- Results of IST Testing
- Failure Analysis
- Statistical Analysis
- Material Ranking
- Conclusions
- Acknowledgements
- Q & A



Introduction

- Results of HDPUG Material Reliability Phase 3
- 12 materials constructed with 2 resin contents
 - High Tg FR4 (2) Halogen Free (6) High Speed (4)
- Materials Characterization Activities:
 - Quantify Impact (Damage?) of 6X passes through 260°C SMT reflow oven
 - PTH via reliability Before and After assembly
 - CAF Resistance
 - Electrical Properties (Dk & Df 1 to 20 GHz)
 - Thermal Properties (TMA & DMA)
- History 98 materials tested to date
- Each phase is completed in 2 years
- Phase 4 now underway 22 New Materials



High Density Packaging User Group (HDPUG) Phase 3 - Lead-Free Study

- Purpose Interconnect Stress Testing (IST) of 24 lead free compatible materials before and after 6X 260°C reflow assembly
- Product Attributes 20 Layers, 2.9mm thick, 0.25mm drilled PTH, 1mm and 0.8mm grids, IAg finish, 2 resin constructions for 12 materials, built by 1 PWB fabricator (Viasystems China)
- Celestica performed 6X Reflows to 260°C, through 10 zone SMT convection oven
- Correlate measured material change with damage found in micro-sections after reflow
- Correlate IST performance with damage found in microsections after reflow



HDPUG Lead-Free Study Responsibilities

- Material Robustness:
 - Confirm Each Material was Produced With Similar Glass/Resin Constructed Materials
 - Determine Variability Across Each Group of Coupons (1mm and 0.8mm Via Spacing)
 - Identify whether Material Damage (Delamination) was created during and/or after 6X 260°C Reflow Cycles
- Via Reliability:
 - Establish baseline performance for 24 constructions, with 2 grid sizes (non-stressed)
 - Test 2nd set of coupons after exposure to 6X 260°C Reflow Cycles (stressed)
 - Complete failure analysis for both copper plating integrity and material robustness
 - Identify whether material damage impacted location or distribution of PTH barrel cracks
 - Rank performance of materials



Test Vehicle Construction

58% Resin Content

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		•					197
PRIMARY	0.5 0Z LYR DI	PREPREG 1 SHEET 1080 GLASS	62% RESIN CONTENT	0027 REF			IP(1
PLANE	1.0 0Z LYR 02	ZZZZ I ANINATE 1 SHEET 2116 GLASS	53% RESIN CONTENT	0050 REE			19134
SIGNAL	1.0 0Z LYR 03	PREPREC 2 SHEETS LOBO CLASS	62% RESIN CONTENT	0054 REE			
PLANE	1.0 0Z LYR 04 -	ZZZZ IAMINATE 1 SHEFT 2116 GLASS	53% RESIN CONTENT	0050 REE		andre Pressent	
SIGNAL	1.0 0Z LYR 05	XXX PREPREC 2 SHEETS 1080 GLASS	627 RESIN CONTENT	0054 REE			
PLANE	1.0 OZ LYR 06	AND AN INATE 1 SHEET 2116 GLASS	53% RESIN CONTENT	0050 REF			
SIGNAL	1.0 0Z LYR 07	XXX PREPREG 2 SHEETS 1080 GLASS	62% RESIN CONTENT	0054 REE			
PLANE	1.0 OZ LYR 08	ZZZ I AMINATE I SHEET 2116 GLASS	53% RESIN CONTENT	0050 REF			17334
SIGNAL	1.0 0Z LYR 09	XXX _ PREPREC 2 SHEETS 1080 CLASS	628 RESIN CONTENT	0054 REF			
PLANE	1.0 0Z LYR 10		EZW RESIN CONTENT	0050 855		many Shanana	224
PLANE	1.0 OZ LYR 11	DECRETA INATE, I SHEET 2110 GLASS	SJA RESTN CONTENT	.0050 REF			
SIGNAL	1.0 0Z LYR 12	VXX PREPREG, Z SHEETS TUBU GLASS	624 RESTN CONTENT	.0034 REF			PI54
PLANE	1.0 0Z LYR 13	ZZZT LAMINATE, I SHEET ZITO GLASS	53% RESTN CONTENT	.0050 REF			
SIGNAL	1.0 0Z LYR 14	PREPREG, 2 SHEETS TUDU GLASS	52% RESTN CONTENT	.0054 REF			DUS TEST IDEA
PLANE	1.D OZ LYR 15	TANINATE, I SHEET 2110 GLASS	SON RESTRICONTENT	0054 REF			Construction of the second
SIGNAL	1.0 0Z LYR 16	XXXX FREE, Z SHEETS TOBU GLASS	538 DECLA CONTENT	.0050 REF			
PLANE	1.0 OZ LYR 17	DECRETARIATE, I SHEET 2110 GLASS	GON DECLN CONTENT	.0054 BEE			
SIGNAL	1.0 0Z LYR 18	ZZZ PREFREG, Z SHEETS 1060 GLASS	538 DEPLN CONTENT	.0054 REF			
PLANE	1.0 OZ LYR 19	DREDREC 1 SHEET 1080 CLASS	62% RESIN CONTENT	0027 REF			
SECONDARY	(0.5 0Z LYR 20 - XXXXXXX	XXXX - THEFHEN, I SHEET TOOD BENSS	VZA NESTR CONTENT	.0027 111			-
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RIMARY	0.5 0Z LYR D1		677 DESIN CONTENT	0030 855			000000000000000000000000000000000000000
PLANE	1.0 0Z LYR 02	TTA I AMINIATE 2 SUFETS 100 OLASS	718 RESIN CONTENT .	0042 REF			C00000000
GIGNAL	1.0 OZ LYR 03 -	DREDREG 2 SHEETS 100 GLASS	67% RESIN CONTENT .	DOGD REF			
LANE	1.0 OZ LYR D4	TALENTRES, 2 SHEETS 106 CLASS	717 RESIN CONTENT .	0042 REF			
IGNAL	1.0 OZ LYR 05	XXX PREPREC 2 SHEETS 1080 CLASS	FTR RESIN CONTENT	0060 REF			
LANE	1.0 OZ LYR 06	ZZZ I ANINATE 2 SHEETS 1060 GLASS	71% RESIN CONTENT	0042 REF	ř.		
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SECTION A-A STACKUP B

ZZZZZZ ZZZ LAMINATE, 2 SHEETS 106 GLASS 71% RESIN CONTENT

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 02
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 71% RESIN CONTENT

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 LYR 10
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 — PREPREC, 2 SHEETS 106 GLASS
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 1.0
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 — LANINATE, 2 SHEETS 106 GLASS
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 — LANINATE, 2 SHEETS 106 GLASS
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 — LANINATE, 2 SHEETS 106 GLASS
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 — LANINATE, 2 SHEETS 106 GLASS
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 LYR 14
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 — LANINATE, 2 SHEETS 106 GLASS
 71% RESIN CONTENT

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 02
 LYR 15
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 — LANINATE, 2 SHEETS 106 GLASS
 71% RESIN CONTENT

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 02
 LYR 16
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 — LANINATE, 2 SHEETS 106 GLASS
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 — LANINATE, 2 SHEETS 106 GLASS
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 — LANINATE, 2 SHEETS 106 GLASS
 71% RESIN CONTENT

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 LYR 16

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SIGNAL

PLANE

LANE

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PLANE

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LANE

SIGNAL

PLANE

1.0 0Z LYR 09-

SECONDARY 0.5 OZ LYR 20 -

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8

0



HDPUG Reflow Oven Profile (6X 260°C)

BTU Pyramax150N 10 Zone Forced Convection Oven

Profile Elements	10 Zone Convection Oven Recommended
Ramp Rate to 217° C Peak	Linear Ramp desired. Can have a small soak period. Usually 1 to 5° C/sec. No more than 2° C/sec
Pre-heat Temperature	Usually measured from 150° C to 200° C. Times within this temperature range are usually 60 to 120 seconds
TAL (Time above 217°C Liquidus)	Target 60 to 90 seconds
Time Within 5° C of Max Peak Temp.	10 to 20 seconds ok. Usually will be lower time.
Target Peak Temperature	260°C Minimum +5°C / -0°C
Ramp Down Rate	Target from 1.5° C/sec to 2.5° C/sec with normal oven cooling configuration
Reflow Atmosphere	Run all samples in air. (Worst case scenario)
Total Time in Oven	Usually 4 to 6 minutes
Thermocouples Attachment	Require minimum of 3 T/C's to properly profile raw card. (Leading Edge + Centre of Card +Trailing edge) are recommended locations.





Capacitance Testing (DELAM)











Capacitance Testing Protocol

- 10 coupons per construction tested non-stressed for 0.8mm & 1mm grids
- 5 coupons from 0.8mm measured after 2nd, 3rd, 4th reflow cycle
- All coupons measured after 6th reflow cycle
- 10 coupons x 2 grids x 24 constructions x 43 readings = 72,000+ data points
- -4% change in bulk capacitance confirms material damage (delamination)



Robust Material Through 6X 260°C



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-A 1

<u>→</u>A 5

-A 7

-A 9

- A 1

📥 A_5 -A 7

-X-A 9

●— A_4 -A 6



Non-Robust Material Through 6X 260°C



Reflow #2

Reflow #4



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Reflow #3



Reflow #6



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Reflow Cycles versus Damage Measured

IST Coupons Exhibiting Material Degradation (Delamination) Between/After 6X 260°C Reflow Cycles												
	2X	3X	4X	6X	6X							
Accomply Loval	Reflow Cycle											
Assembly Level	(Out of 5)	(Out of 5)	(Out of 5)	(Out of 8)	Only							
	Minimum	Standard	One Rework	BGA Rework	BGA Rework							
Material Code		.032" / 0.8m	nm Coupons		.040" / 1mm							
		FR4:										
Α	0	0	0	0	No							
AB	0	0	0	0	No							
В	0	0	0	0	No							
BB	0	0	0	0	No							
		Halogen Fre	ee FR4:									
C	0	40%	80%	88%	No							
СВ	0	80%	80%	100%	No							
D	0	20%	40%	100%	No							
DB	0	0	60%	100%	Yes							
E	0	0	0	0	No							
EB	0	0	20%	100%	Yes							
F	100%	100%	100%	100%	Yes							
FB	100%	100%	100%	100%	Yes							
G	0	40%	40%	50%	No							
GB	0	20%	80%	100%	Yes							
Н	0	0	0	0	No							
HB	0	0	0	0	No							
		High Speed N	laterials:									
Ι	0	0	0	100%	No							
IB	0	20%	100%	100%	Yes							
J	0	60%	100%	100%	No							
JB	100%	100%	100%	100%	Yes							
K	0	0	0	65%	No							
KB	0	0	0	88%	No							
L	0	0	0	0	No							
LB	0	0	0	0	No							
Defective Materials	3	10	12	15	8							



Material Damage After 6X 260°C

Presence of Material Damage												
Material Type	.032" Grid	.040" Grid										
	FR4:											
А	None	None										
AB	None	None										
В	None	None										
BB	None	None										
H	Halogen Free FR4:											
С	Present	None										
CB	Present	None										
D	Present	None										
DB	Present	Present										
E	None	None										
EB	Present	Present										
F	Present	Present										
FB	Present	Present										
G	Present	None										
GB	Present	Present										
Н	None	None										
HB	None	None										
Hig	gh Speed Materials:											
Ι	Present	None										
IB	Present	Present										
J	Present	None										
JB	Present	Present										
K	Present	None										
KB	Present	None										
L	None	None										
LB	None	None										
Damaged Material	15/24	8/24										





Correlation Between DELAM and X-section

ECWC13 Code	DELAM 1mm	X section 1mm	Match	DELAM 0.8mm	X section 0.8mm	Match
			FR4:			
А	No	No		No	No	
AB	No	No		No	No	
В	No	No		No	No	
BB	No	No		No	No	
		Halo	gen Free	FR4:		
С	No	Minor		Yes	Yes	
CB	No	Minor		Yes	Yes	
D	No	Yes	No Yes	Yes	Yes	
DB	Yes	Yes		Yes	Yes	
E	No	No		No	No	
EB	Yes	Yes		Yes	Yes	
F	Yes	Yes		Yes	Yes	
FB	Yes	Yes		Yes	Yes	
G	No	No		Yes	Yes	
GB	Yes	Yes		Yes	Yes	
Н	No	No		No	No	
HB	No	No		No	No	
		High S	Speed Mat	erials:		
	No	Minor		Yes	Yes	
IB	Yes	Yes		Yes	Yes	
J	No	No		Yes	Yes	
JB	Yes	Yes		Yes	Yes	
K	No	No		Yes	Yes	
KB	No	Minor		Yes	Yes	
L	No	No		No	No	
LB	No	No		No	No	
Results	23 Ma	atch 1 No I	Match	24 Ma	atch 0 No M	latch

DELAM Achieved 98% Correlation to X-Section



ions inc. S and services Correlation Between Reflow Oven versus 6X 288°C Solder Float

6X 288° C Solder Float Achieved 58% Correlation to Reflow Oven

	0.8mm/.032" 1mm/.040"												
		7	0.8mm	17.032"		7	1mm/	.040"					
EDMCI3 Come	6X 260C SMT REFLOW OR 6X 288C SOLDER FLOAT	Hde Cty Examinac	(31) malad	DaanOrades	uprew	Hde Cty Examinac	Dalam(8)	DaanOrades	uprew				
А	6X Reflow	13	no	0		11	no	0					
AB	6X Reflow	16	no	0	No	12	no	0					
в	6X Reflow	15	no	0		12	no	0					
	6X Solder Float 6X Reflow	<u>24</u> 16	no no	0		<u>19</u> 13	no no	0					
вв	6X Solder Float	23	Yes	1	NO	19 11	no	0					
С	6X Solder Float	24	no	0	No	20	no	0					
СВ	6X Reflow 6X Solder Float	16 24	Yes Yes	14		14 19	no no	0					
D	6X Reflow	14	Yes	17		12	Yes	10	No				
DB	6X Reflow	15	Yes	13	No	12	Yes	7	No				
F	6X Solder Float 6X Reflow	14	no	0		<u>19</u> 13	no no	0					
	6X Solder Float	24	no	0		<u>20</u>	no	0					
EB	6X Solder Float	24	no	0	No	19	no	Ŏ					
F	6X Reflow 6X Solder Float	14 23	Yes Yes	18 21		13 18	Yes Yes	12 28					
FB	6X Reflow	15	Yes	23		12	Yes	13					
G	6X Reflow	15	Yes	13		13	no	0	No				
-	6X Solder Float 6X Reflow	<u>23</u> 15	Yes Yes	<u>21</u> 15		<u>18</u> 12	Yes Yes	2					
GB	6X Solder Float	23	Yes	1		19	no	0	NO				
н	6X Solder Float	15 24	no no	0		12	no no	0					
нв	6X Reflow 6X Solder Float	15	no	0		13	no	0					
I	6X Reflow	15	Yes	15	No	12	no	0					
IB	6X Reflow	15	Yes	15	No	13	Yes	6	No				
10	6X Solder Float	24 15	no Yes	0		18 14	no	0					
J	6X Solder Float	23	no	0	No	18	no	Ő					
JB	6X Reflow 6X Solder Float	16 24	no	18 0	No	13 19	res no	13 0	No				
к	6X Reflow	16	no Yes	0	No	13	no	0					
КВ	6X Reflow	16	no	0		12	no	0					
<u> </u>	6X Reflow	15	no	0		19	no	0					
	6X Solder Float	24	no	0		20	no	0					
LB	6X Solder Float	23	no	0		19	no	0					
Results 14 Match 10 No Match 18 Match 6 No Match									atch				



0.8mm Material Damage Crack Count

	Crack Count vs. Electrical Data on .032"/0.8mm Grid Coupons																																			
Layer		2/4				4/6				6/8			5	8/1	0		1	0/1	1		1	1/1	.3		1	3/1	5		1	5/1	.7		1	7/1	9	
R32 Coupons	S	М	L		S	М	L		S	М	L		S	М	L		S	М	L		S	М	L		S	М	L		S	М	L		S	М	L	
А	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
AB	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
В	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
BB	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
С	0	0	0		0	0	0		0	0	0		0	0	8	>	1	0	0	>	0	0	23	>	0	8	0	>	0	0	0		0	0	0	
СВ	0	0	0		0	0	0		2	0	2	>	0	1	28	>	0	0	0		2	0	1	>	0	0	1	>	0	0	0		0	0	0	
D	0	0	0		0	0	0		6	1	0	1	0	2	10	✓	0	0	10	✓	1	0	3	>	0	0	0		0	0	0		0	0	0	
DB	0	0	0		0	0	0		0	1	0	>	0	2	14	>	0	2	3	✓	0	5	16	>	0	5	1	>	0	0	0		0	0	0	
E	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
EB	0	0	0		0	0	0		0	4	4	>	0	0	18	>	0	0	0		2	0	19	>	5	0	9	>	0	0	0		0	0	0	
F	0	0	0		10	0	0	x	0	6	7	1	0	3	12	✓	0	0	0		0	0	32	>	12	0	0	✓	0	0	0		0	0	0	
FB	13	0	0	X	22	2	0	X	13	0	3	>	0	2	14	>	0	0	0		0	3	20	>	4	0	0	>	0	0	0		0	0	0	
G	0	0	0		0	0	0		0	0	0		0	5	9	>	0	3	4	>	0	0	7	>	2	1	2	>	0	0	0		0	0	0	
GB	0	0	0		0	0	0		12	4	1	1	0	2	25	✓	0	1	3	✓	0	12	7	✓	7	0	0	✓	0	0	0		0	0	0	
Н	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	0	0	0	0		0	0	0		0	0	0		0	0	0	
HB	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	0	0	0	0		0	0	0		0	0	0		0	0	0	
I	0	0	0		0	0	0		1		1	>	0	0	5	>	0	0	0	0	0	3	10	>		0	5	>	0	0	0		0	0	0	
IB	0	0	0		0	0	0		0	4	5	>	0	6	18	>	7	0	1	✓	0	0	28	>	2	0	0	>	0	0	0		0	0	0	
J	0	0	0		0	0	0		0	0	6	>	27	0	0	>	19	0	0	✓	0	0	31	>	7	0	0	>	0	0	0		0	0	0	
JB	0	0	0		0	0	0		8	1		>	32	0	0	>	23	0	0	>	1	0	27	>	0	0	7	>	0	0	0		0	0	0	
К	0	0	0		0	0	0		0	0	0		6	0	7	✓	1	0	0	✓	0	0	12	-	0	0	12	✓	0	0	0		0	0	0	
КВ	0	0	0		0	0	0		1	0	0	✓	15	0	2	✓	0	0	0		0	0	31	✓	2	0	0	✓	0	0	0		0	0	0	
L	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
LB	0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0		0	0	0	
Note:	А	che	ck i	mar	k 🗸	inc	lica	tes	the	der	nag	eir	the	e mi	cro	sec	tion	an	d th	e el	ecti	rica	l da	ma	ge a	agre	e. A	An X	inc	lica	tes	a di	isag	gree	ment	t.



Material Damage Crack Count





Cohesive Damage by Glass Style/Type



Material	5	8%	69	9%
Туре	C=1X 2116	B= 2X 1080	C= 2X 106	B= 2X 1080
С		x		
СВ				x
D	x			
DB			x	x
EB			x	
F		x		
FB				x
G	x	x		
GB			x	x
	x	x		
IB			x	х
J		x		
JB				x
K		x		
KB				x



Impact of 0.8mm Vs 1mm Grid Size



Note: The severity of damage found on 0.8mm was 2X the level found on 1mm



Why is 0.8mm grid more susceptible to material damage?

When the structure of the composite materials reaches a specific temperature an internal shear stress is generated by the mis-match of CTE. The CTE mismatch is caused by the combination of the strength of the glass restricting the x axis expansion, versus the non-restricted expansion of the resin in the y axis. The focal point of this CTE mismatch is located at the "knuckle" between the woven glass fabrics, this is premised on the examination of microsections that consistently exhibit material cracks at the cross-over point between the warp and the weft glass directions.



I.S.T. Accelerated Reliability Testing





6X 260°C Reflow Cycles Caused Damage!

	Capacitan Indicates Damag 6X 2600	ce Testing Material ge After C Reflow	Micros Indicates Damag 6X 2600	ection Material Je After Reflow		
SMTAI CODE	DELAM 1mm	DELAM 0.8mm	X section 1mm	X section 0.8mm		
	ŀ	ligh Tg FR	4			
Α	No	No	No	No		
AB	No	No	No	No		
В	No	No	No	No		
BB	No	No	No	No		
	н	alogen Fre	e			
С	No	Yes	Minor	Yes		
СВ	No	Yes	Minor	Yes		
D	No	Yes	Yes	Yes		
DB	Yes	Yes	Yes	Yes		
E	No	No	No	No		
EB	Yes	Yes	Yes	Yes		
F	Yes	Yes	Yes	Yes		
FB	Yes	Yes	Yes	Yes		
G	No	Yes	No	Yes		
GB	Yes	Yes	Yes	Yes		
н	No	No	No	No		
HB	No	No	No	No		
	Hig	gh Speed F	R4			
I	No	Yes	Minor	Yes		
IB	Yes	Yes	Yes	Yes		
J	No	Yes	No	Yes		
JB	Yes	Yes	Yes	Yes		
K	No	Yes	No	Yes		
KB	No	Yes	Minor	Yes		
L	No	No	No	No		
LB	No	No	No	No		
	Minor	= Not Reje	ectable Dar	nage		



Presence of Material Damage												
Material Type	.032" Grid	.040" Grid										
	FR4:											
А	None	None										
AB	None	None										
В	None	None										
BB	None	None										
ŀ	lalogen Free FR4:											
С	Present	None										
СВ	Present	None										
D	Present	None										
DB	Present	Present										
E	None	None										
EB	Present	Present										
F	Present	Present										
FB	Present	Present										
G	Present	None										
GB	Present	Present										
Н	None	None										
HB	None	None										
Hig	gh Speed Materials:											
	Present	None										
IB	Present	Present										
J	Present	None										
JB	Present	Present										
K	Present	None										
KB	Present	None										
L	None	None										
LB	None	None										
Damaged Material	15/24	8/24										



Problem Statement

• The basis of a successful PTH via reliability study is built upon the premise that material integrity is not compromised, and an assurance that fatigue in the central zone of the PTH barrel is the only failure mode.



IST Testing Protocol

• Cycle between ambient and 150°C in 3 min's, cool to ambient in 2 min's, reject at 10% (IPC) increase in resistance

• IST test 6 coupons, superheat designed with the 0.8mm and 1mm grids, for 24 constructions tested in the non-stressed condition

- All materials received 6X 260°C reflow cycles
- IST test 2nd set of 6 coupons of each grid/ construction tested in the stressed condition
- Failure analysis completed on 1 coupon from each grid size, test condition and construction
- IST results statistically compared (24 builds x 2 grid sizes x 2 test conditions x 6 coupons = 576 test coupons



Resistance Degradation After 6X 260°C







		1mm/0.0	40" Grid			0.8mm/0.	032" Grid	
ECWC13 Coding	IST 1mm As Built	IST 1mm after 6X 260C	Damage - 1mm	1mm 6X Compare better than AB?	IST 0.8mm As Built	IST 0.8mm after 6X 260C	Damage - 0.8mm	0.8mm 6X Compare better than AB?
		High Tg FR	4			High 1	「g FR4	
Α	677	513	No	No	699	521	No	No
AB	447	358	No	No	420	362	No	No
В	372	256	No	No	332	228	No	No
BB	380	173	No	No	386	201	No	No
	H	lalogen Fre	e			Haloge	en Free	
С	993	568	No	No	932	628	Yes	No
СВ	768	393	No	No	805	598	Yes	No
D	516	332	Yes	No	566	289	Yes	No
DB	490	378	Yes	No	499	642	Yes	Yes
E	173	43	No	No	169	16	No	No
EB	115	42	Yes	No	109	53	Yes	No
F	280	527	Yes	Yes	259	558	Yes	Yes
FB	235	381	Yes	Yes	223	260	Yes	Yes
G	>2000	1269	No	No	>2000	1753	Yes	No
GB	>2000	1217	Yes	No	1860	2000	Yes	Yes
Н	>2000	>2000	No	No	>2000	1860	No	No
HB	1906	1157	No	No	1955	1032	No	No
	Hi	gh Speed F	R4			High Sp	eed FR4	
I	1040	576	No	No	962	760	Yes	No
IB	819	374	Yes	No	757	756	Yes	No
J	434	191	No	No	404	333	Yes	No
JB	302	224	Yes	No	280	331	Yes	Yes
K	821	335	No	No	768	392	Yes	No
KB	602	382	No	No	623	385	Yes	No
L	>2000	1703	No	No	>2000	1859	No	No
LB	>2000	1567	No	No	>2000	1730	No	No



Relative Performance of 24 Constructions





Cu Fatigue Cracks Moved Away From Damage!





0.8mm Non Stressed Vs Stressed

Material Damage Included

Material Damage Removed





1mm Non Stressed Vs Stressed

Material Damage Included

Material Damage Removed





0.8mm + 1mm Non Stressed Vs Stressed

Material Damage Included

Material Damage Removed





Ranking FR4 Performance

	High Tg FR4												
Rankin	g of Non-st	ressed	Rank	Ranking of Stressed									
Coupor	ns With Bot	h Grids	Coupons With Both Grids										
Coupon	Log N	Delam	Coupon	Coupon Log N [
A	646	No	A	453	No								
AB	402	No	AB	337	No								
BB	355	No	В	219	No								
В	310	No	BB	155	No								

Ranking Halogen Free Performance

Halogen Free											
Ranking of Non-stressed			Ranking of Stressed			Ranking of Stressed			Ranking of Stressed		
Coupons With Both Grids			Coupons With Both Grids			1mm/0.040" Coupons Only			Coupons With Both Grids		
Coupon	Log N	Delam									
G	2000	No	Н	2000	No	Н	2000	No	Н	2000	No
GB	2000	No	G	1533	Yes	HB	910	No	HB	925	No
Н	2000	No	GB	1340	Yes	G	869	No	E	25	No
HB	1873	No	HB	925	No	С	458	No			
С	852	No	С	498	Yes	CB	341	No			
CB	730	No	F	448	Yes	E	40	No			
D	482	No	DB	436	Yes				_		
DB	457	No	CB	433	Yes						
F	245	No	FB	271	Yes						
FB	203	No	D	265	Yes						
E	160	No	EB	39	Yes						
ËB	104	No	E	25	No						



Ranking High Speed FR4 Performance

High Speed FR4											
Ranking of Non-stressed			Ranking of Stressed			Ranking of Stressed			Ranking of Stressed		
Coupons With Both Grids			Coupons With Both Grids			1mm/0.040" Coupons Only			Coupons With Both Grids		
Coupon	Log N	Delam									
L	2000	No	L	1713	No	L	1607	No	L	1713	No
LB	2000	No	LB	1532	No	LB	1383	No	LB	1532	No
I	940	No	Ι	594	Yes	I	505	No			
IB	745	No	IB	460	Yes	KB	339	No			
K	744	No	KB	345	Yes	K	285	No			
KB	591	No	K	327	Yes	J	173	No			
J	389	No	JB	240	Yes						
JB	268	No	J	215	Yes						



Material Robustness Conclusions

• Fifteen of the 24 materials proved unsuitable after 6X 260°C Pb free assembly, specifically on the 0.8mm/.032" grid size. Eight materials proved unsuitable on the 1mm/.040" grid size.

• Three "Pb free compatible" materials demonstrated delamination in the 2nd cycle of assembly, 10 materials delaminated in the 3rd cycle. 12 materials delaminated in the 4th cycle Each preconditioning cycle produced increasing levels of material damage.

•Material damage through Pb free assembly was dominated by cohesive failure, primarily across the central zone of the construction.

•The nature of the cohesive damage is compromising the critical glass/resin interface. Laminate manufacturers must investigate this situation to understand root cause and introduce improvements.



Material Robustness Conclusions Con't

• The MRT-5 IST test coupon design and DELAM testing protocol proved very effective at characterizing the presence, location and magnitude of material damage during and after Pb free assembly, achieving a 98% confidence when compared with microsection analysis.

•The electrical specification based on a minimum of 4% decrease in bulk capacitance demonstrated the ability to identify and confirm material damage.

•The results of conventional 6X solder float testing to 288°C did not achieve statistical correlation (58%) with coupons that received 6X 260°C Pb free reflow assembly.

•The majority of damage caused during assembly was focused toward the centre of the construction. The material damage was not visible on the surface layers, although major delamination was present throughout the construction.



IST Accelerated Reliability Conclusions

• IST results ranged from immediate failures to no failures found at 2000 cycles. This is based on identical electrolytic copper plating conditions for all constructions

• Cohesive material damage was demonstrated to be stress relieving, the areas of copper cracks, effectively redistributing the strain into different locations within the construction.

• There were 7 instances (out of 24) where PTH via reliability performances were increased following exposure to 6X 260°C reflow cycles, compared to non-stressed results. The combined effects of stress redistribution and stress relieving across the central zone of the copper plated barrel are considered to be the primary explanation.



Overall Study Conclusions

• Any future PWB PTH thermal cycling reliability studies that combines a grid size of 1mm/0.040 or smaller, and will apply multiple exposures to Pb-free reflow assembly must anticipate the requirement to quantify the presence of material damage in their testing protocols.

• Material suitability for Pb-free assembly reflow cannot be determined by visual inspection alone. Applying methodologies like DELAM testing is a complementary strategy to identifying material damage in test vehicles.

• The majority of cohesive damage was found in the same location of the construction, where copper fatigue cracks were found to initiate and propagate.



Overall Study Conclusions (Cont'd)

• Grid sizes of 0.8mm/0.032" are 2X more susceptible to cohesive material damage during multiple Pb-free reflow cycles compared to 1mm/0.040". Fifteen out of 24 materials exhibited multiple levels of cohesive delamination in 0.8mm/0.032" coupons compared to "only" 8 materials in 1mm/0.040" coupons.

• Quantifying the overall PTH via reliability performance proved difficult when attempting to make a material ranking, due to the confounded effects of cohesive material damage.

• In the ranking system demonstrated in this study equal importance was applied to both the performance of via reliability and material integrity.



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- Statistical Analysis
- Failure Analysis
- DMA Thermal Analysis
- Report Writing

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Thank you for your attention!

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