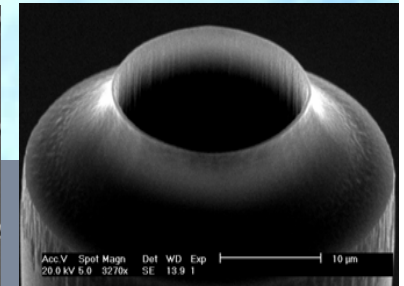
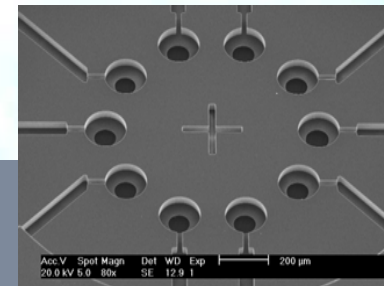
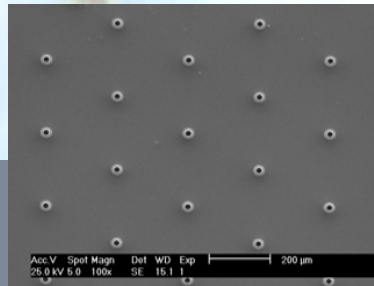


# Integrated Electrospray Micropropulsion System

R. Krpoun (Renato.krpoun@epfl.ch) and H. Shea (herbert.shea@epfl.ch)

Microsystems for Space Technologies Laboratory  
EPFL, Lausanne  
Switzerland



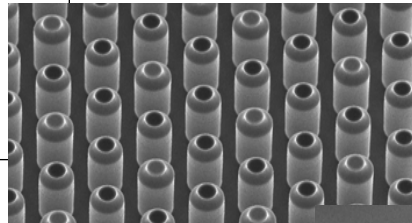
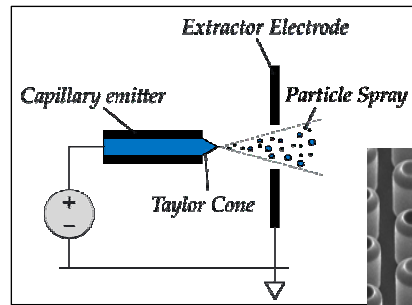
## Acknowledgments

The authors would like to thank:

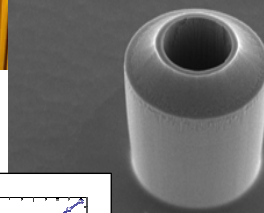
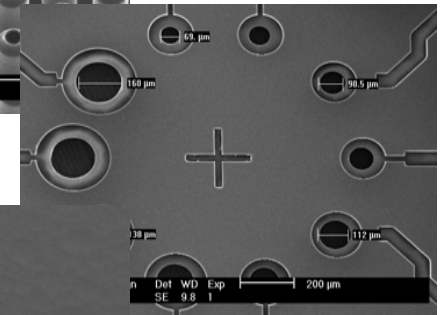
- ESA and Mr. José González del Amo for support (ESA ITI Type A - Contract No 20022/06/NL/PA)
- Katharine Smith & John Stark at Queen Mary, University of London, United Kingdom for very valuable inputs during the development of the thrusters
- the staff of the EPFL-CMI and the University of Neuchâtel COMLAB for their help during device fabrication.

# Outline

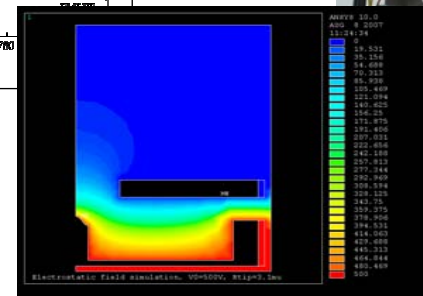
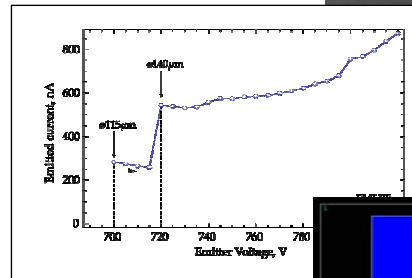
- Introduction
- Thruster Design
- Microfabrication
- Experimental Details
- First Results
- Conclusion and outlook



Spot Magn Det WD Exp  
5.0 339x SE 13.2 1 ES-05-01 W2

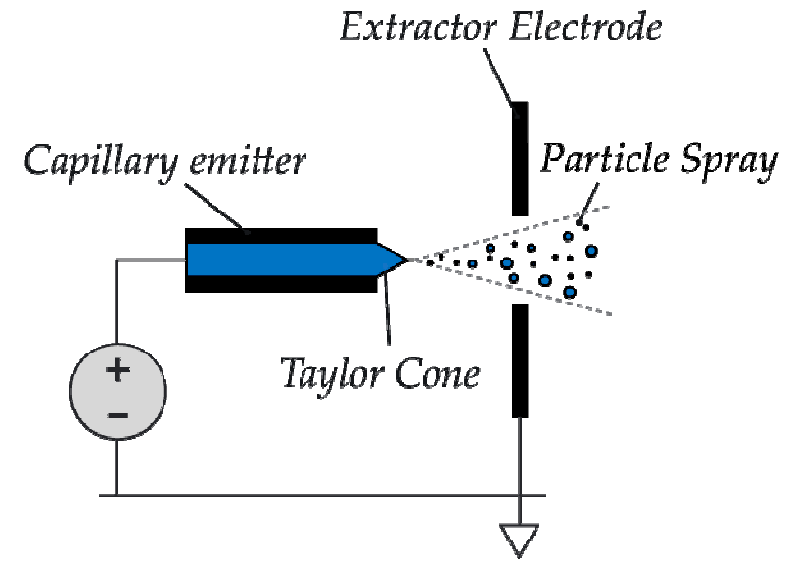


Spot Magn Det WD Exp  
9x SE 9.2 1



## Introduction to Electro spray Electrosprays

- Principle of operation:** a liquid at the tip of a capillary is electrically charged to a high voltage. Above a critical threshold the liquid deforms into a cone and a spray of charged droplets or ions is accelerated towards an extractor electrode.
- Several research groups have observed transition from **ions to droplets** in sprays when using ionic liquids as fuel.
- In ionic mode a **large Isp** ( $> 1000s$ ) can be reached, but thrust is low thus the **motivation of having arrays of emitters.**



$$I_{sp} = \frac{1}{g} \sqrt{2V_a \frac{q}{m}}$$

Specific impulse

$$T = I \frac{m}{q} \sqrt{2V_a \frac{q}{m}}$$

Thrust

|       |                        |
|-------|------------------------|
| $q$   | charge                 |
| $m$   | particle mass          |
| $V_a$ | applied voltage        |
| $I$   | current                |
| $g$   | gravitational constant |

## Propulsion requirements – future ESA missions

| Parameter                 | Value                                 |
|---------------------------|---------------------------------------|
| Thrust                    | 1 $\mu\text{N}$ to 1 mN               |
| Thrust noise              | $< 0.1 \mu\text{N} / \text{Hz}^{1/2}$ |
| Mass                      | minimize                              |
| Isp                       | $> 4000 \text{ s}$                    |
| Thrust resolution         | $< 0.1 \mu\text{N}$                   |
| Thrust linearity          | $< 4 \mu\text{N} \pm 4\%$             |
| Thrust repeatability      | $< 0.5 \mu\text{N} \pm 0.5\%$         |
| Lifetime                  | $> 10'000 \text{ hours}$              |
| Thrust vector instability | minimize                              |

Introduction

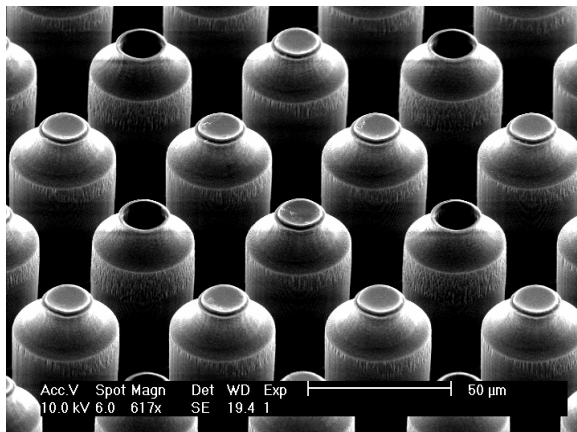
# Micro-Fabrication – Advantages (1)

- **Scalability** – with MEMS technology large arrays can be microfabricated (easily covering 100 cm<sup>2</sup>) to increase thrust
- **Redundancy**: if a few emitters in an array fail, the thruster continues to operate
- **Low voltage**: the very small spacing  $l$  (<25 μm) between ion source and extraction electrodes which, coupled with small capillary diameter  $d$ , can decrease to under 500 V the voltage required to spray from a Taylor cone.

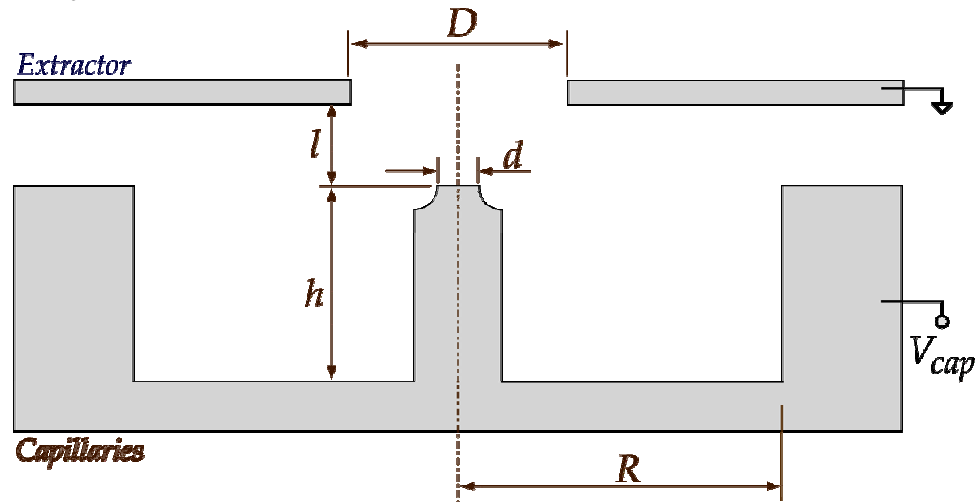
Starting voltage (approximation)

$$V_{oc} \approx \sqrt{\frac{\gamma \cdot d}{2 \cdot \epsilon_0}} \cdot \ln \left[ \frac{2l}{d} \right]$$

[Ref. Martínez-Sánchez, MIT Open Courseware]



Microfabrication test

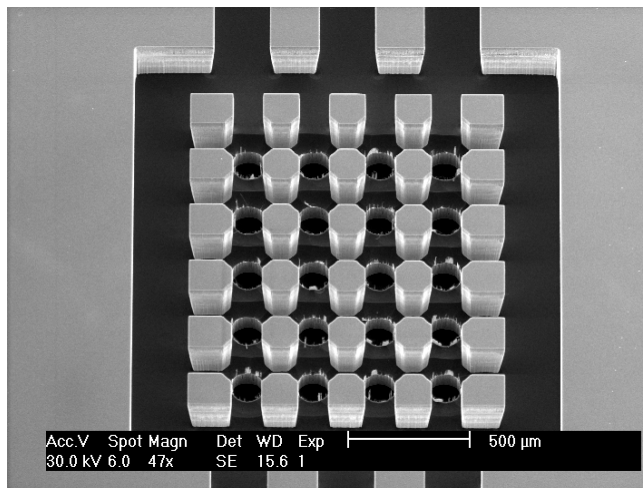


Geometry of prototype thruster

## Introduction

## Micro-Fabrication – Advantages (2)

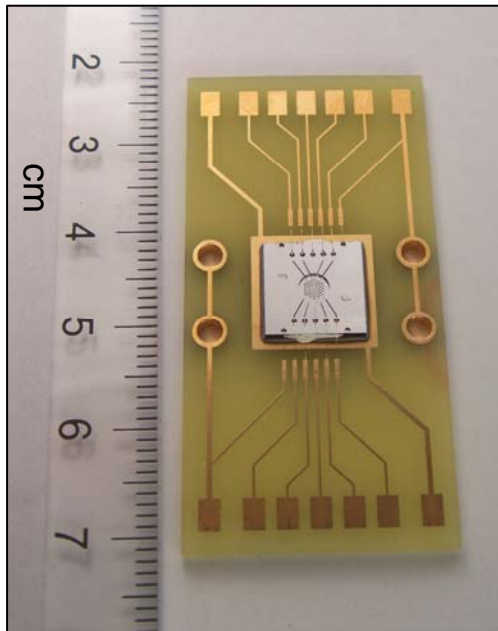
- **No moving parts:** all thrust control is done by changing voltages on extraction and acceleration electrodes.
- **Large thrust range**
  - by continuously going from ionic mode to droplet mode: can choose between high mass or high power efficiency.
  - By emitting only from selectable subset of capillaries
- Fluidic network can be **integrated** in the back of the chip: no pumping



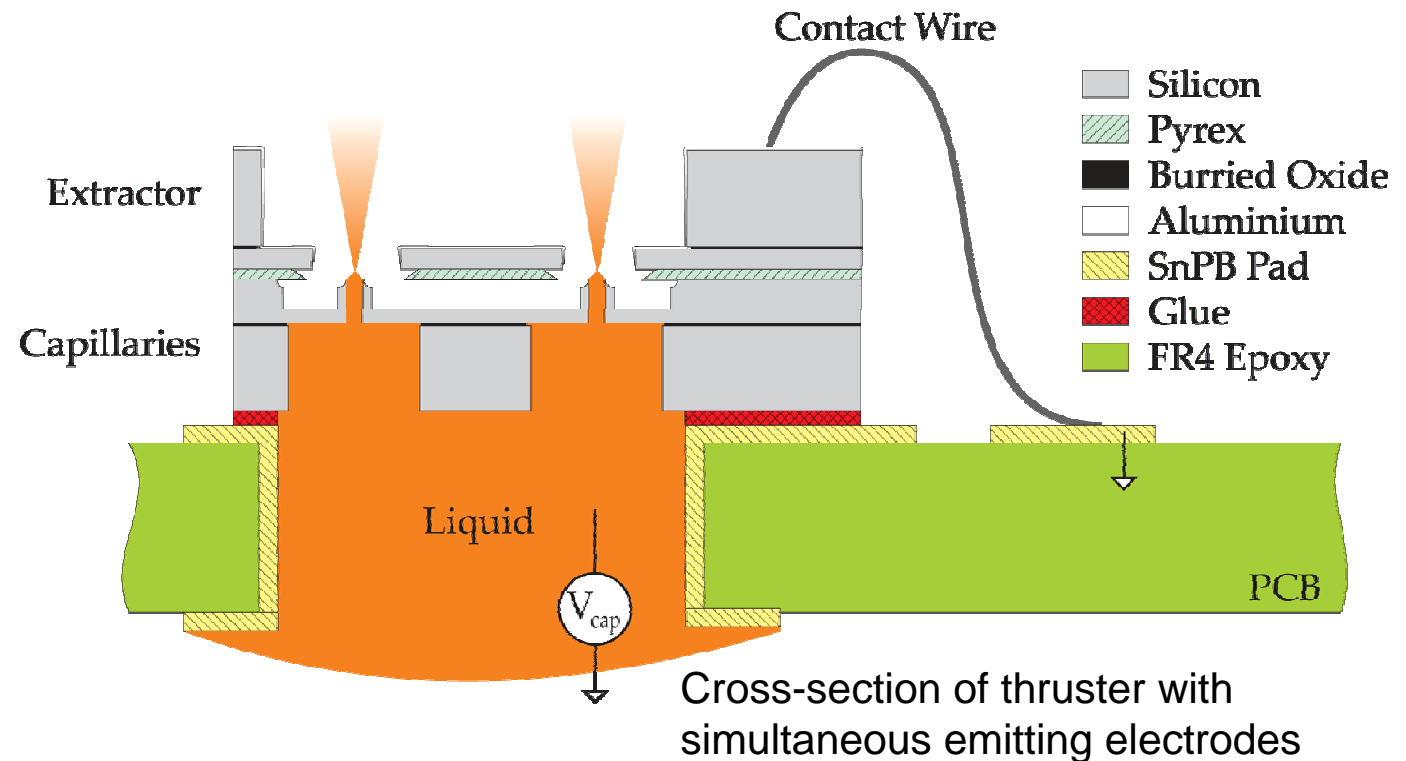
SEM image of a fluid handling system on the back of a capillary chip

# Thruster Design: Overview

- Each capillary emitter has an **individual extractor** electrode. Two designs:
  - All extractors in parallel (same voltage on all)
  - Individually addressable extractor electrodes to spray from any given capillary
- For vacuum testing the microfabricated thruster is mounted on a PCB.
- **No active pumping** is necessary, wetting of structures occurs through capillarity.

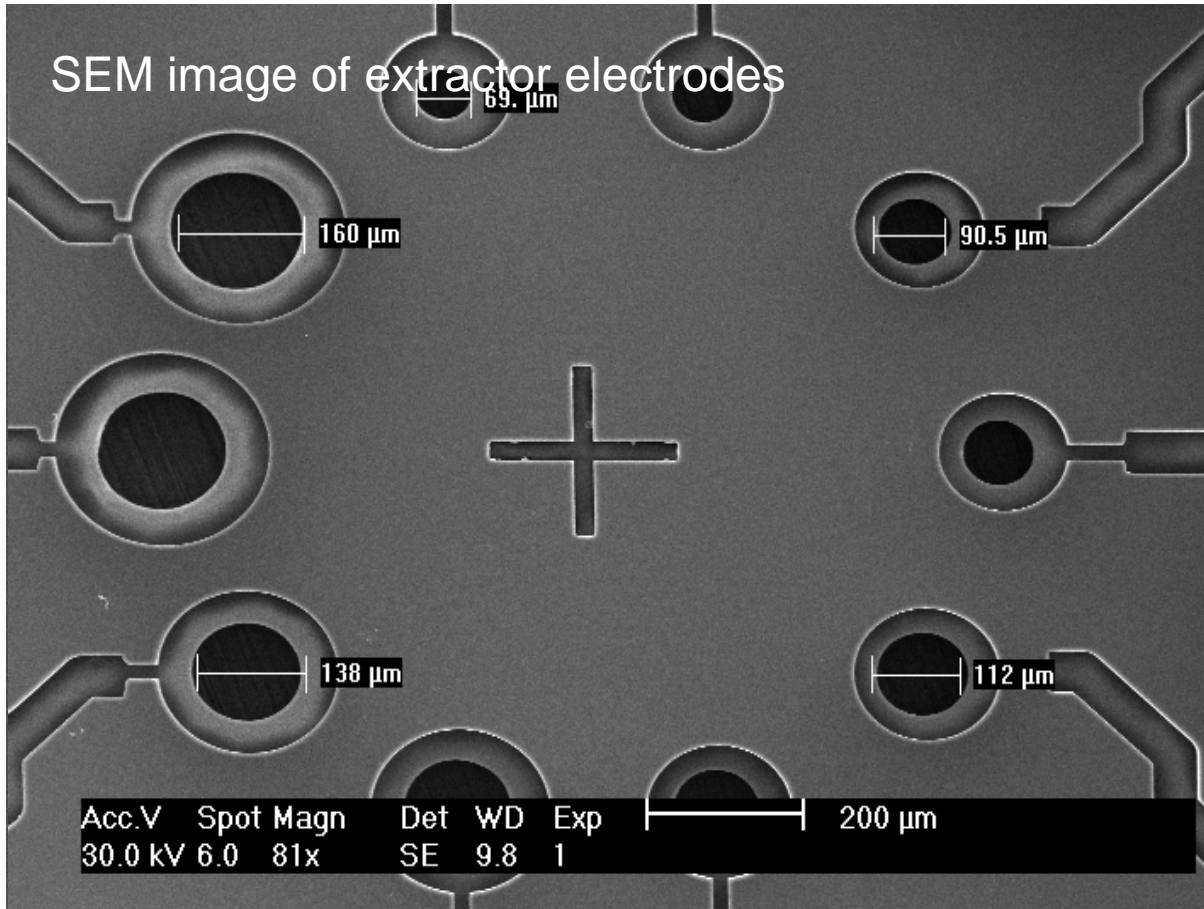


thruster assembly

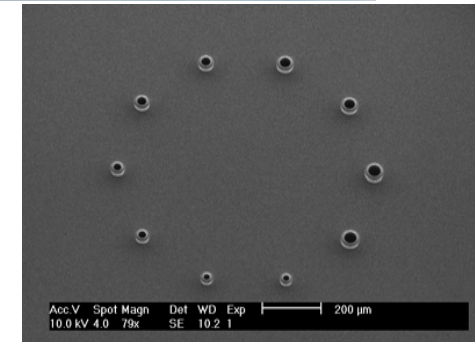




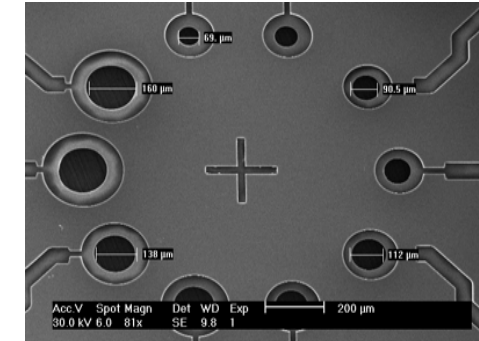
# Thruster Design: Geometry and Wafer Layout



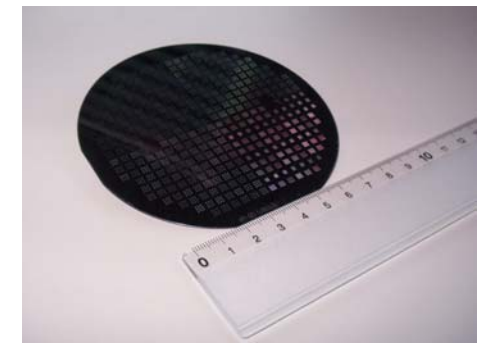
Thruster cross section with standard dimensions



Capillaries, various diameters



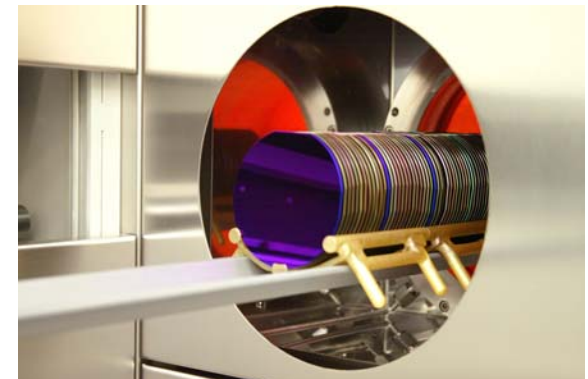
Extractors, various diameters



4" wafer

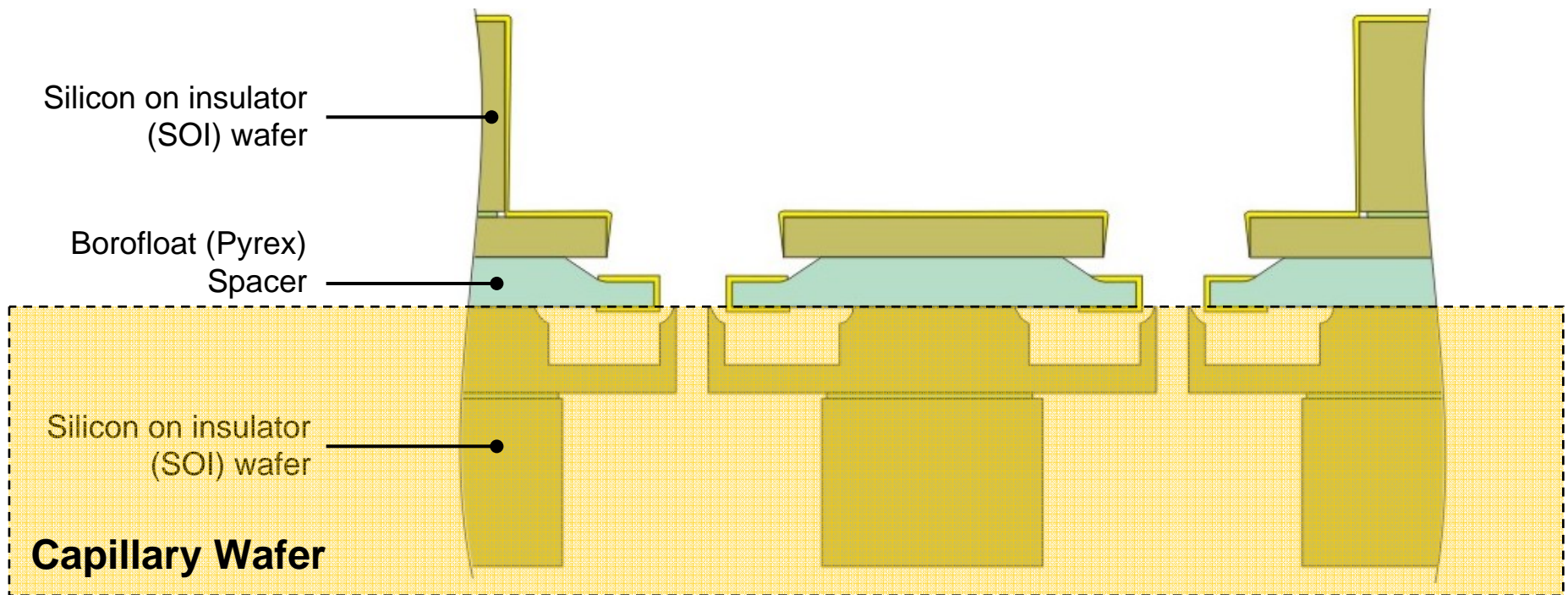
## Microfabrication Facilities

- Access to two state-of-the-art MEMS cleanroom facilities:
  - COMLAB (Neuchâtel)
  - CMI/EPFL (Lausanne)
- For quality assurance, debugging and process development, access to the following tools is available (in Neuchâtel and Lausanne):
  - Scanning Electron Microscopes (including ESEM, EDX, BSE ...)
  - Transmission electron microscope (including FIB for sample preparation)
  - Various optical microscopes for process control and thin film characterization
  - Etc.



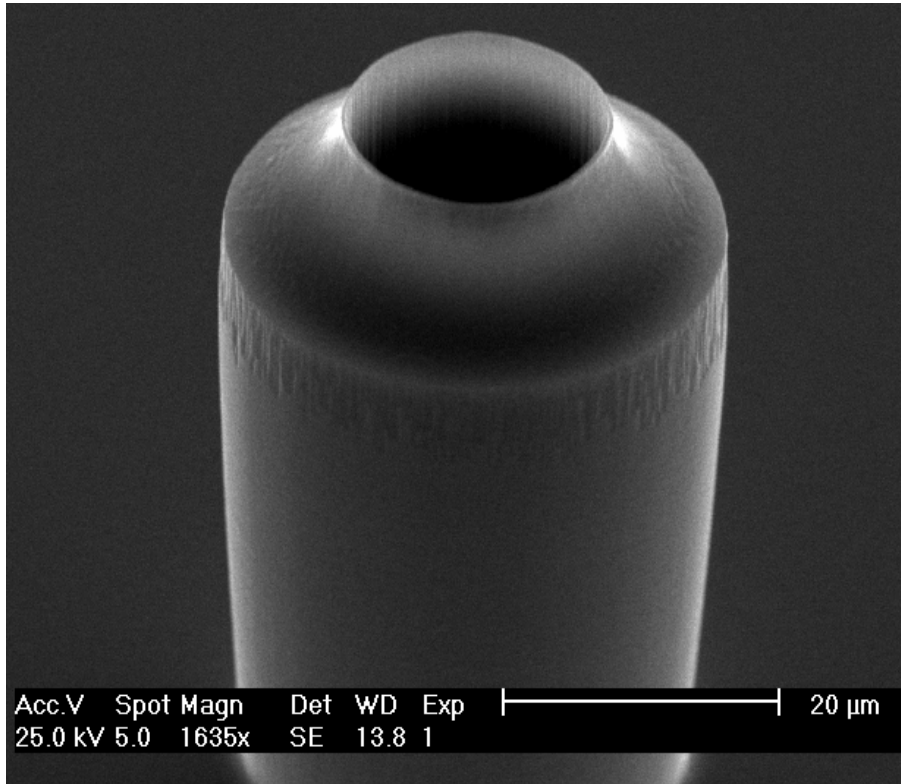
## Microfabrication Process Flow – Capillary Arrays

- Two distinct elements have been developed
  - Capillary Emitters  
(modification of a design by Griss, *et al.*, J. Micromech. Microeng. **12** (2002), pp. 682–687)
  - Extractor electrodes
- The design allows to stack further electrostatic lens components

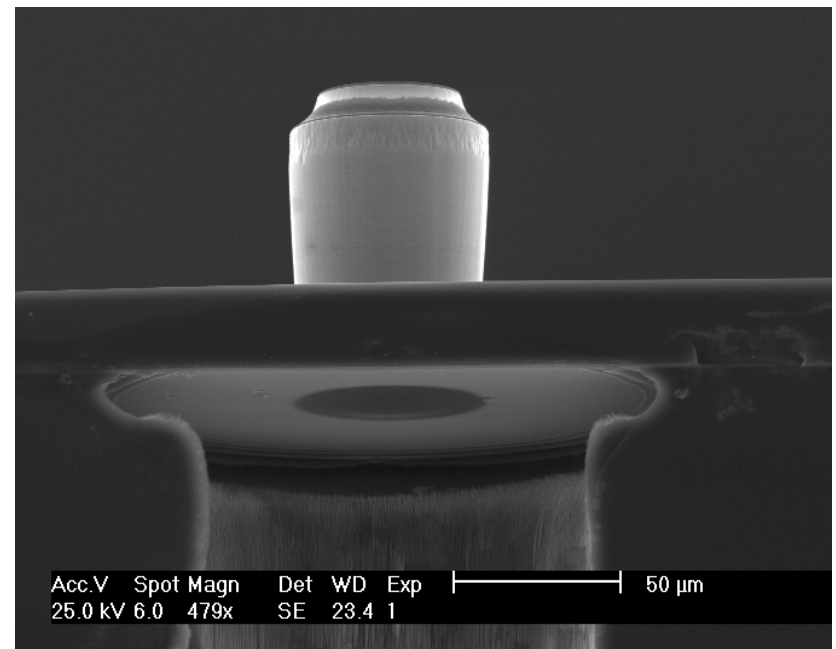
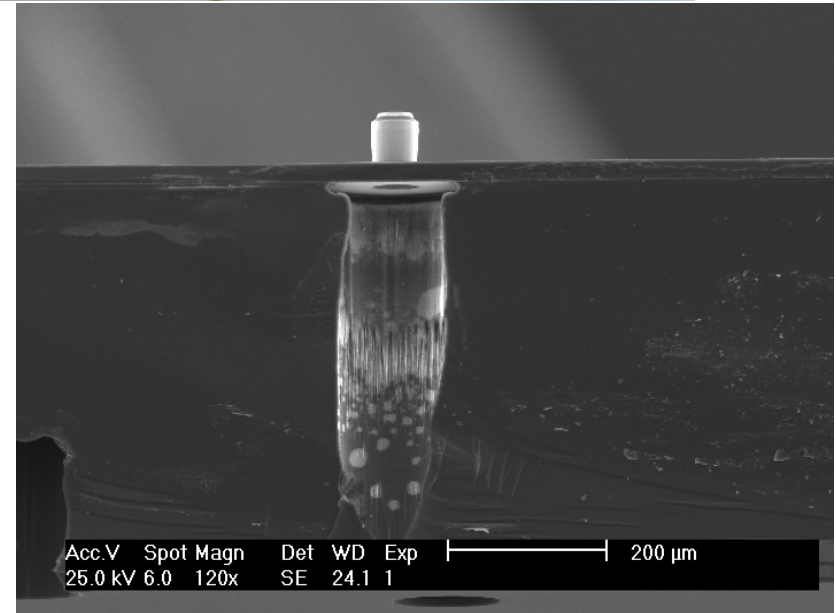


Thruster assembly with individually addressable extractor electrodes

# Microfabrication Capillaries



SEM images of a capillary emitter



Microfabrication  
Process Flow – Extractor Arrays

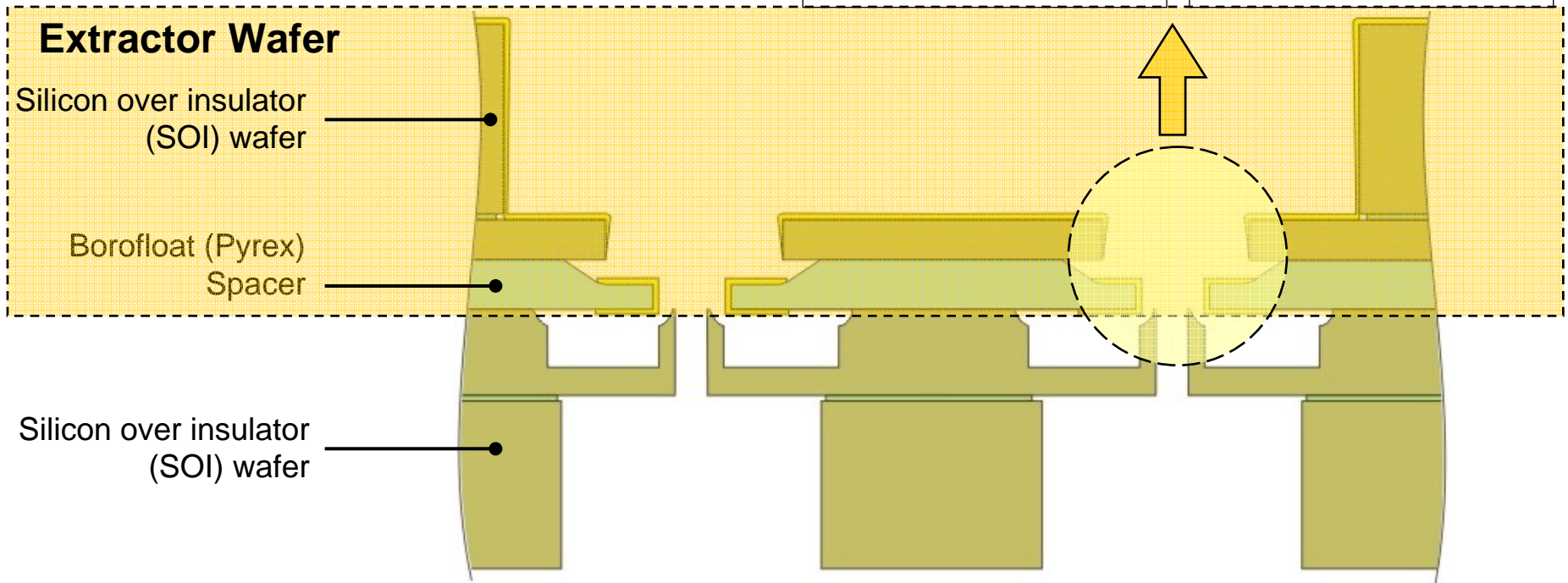
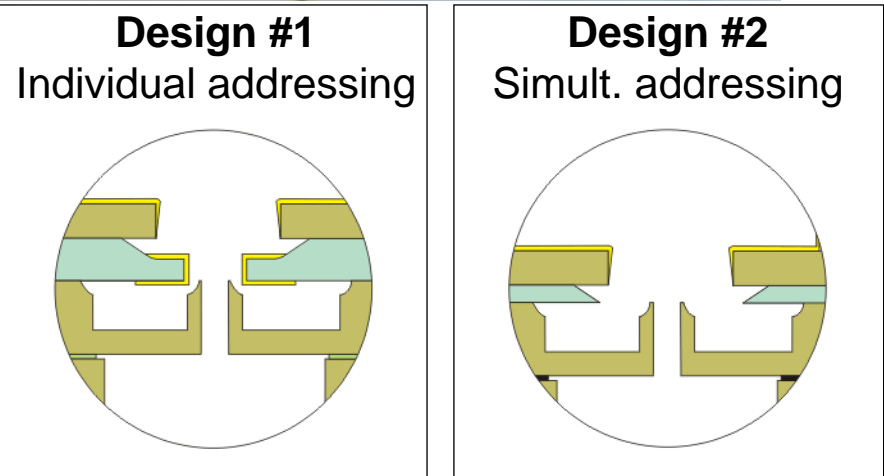
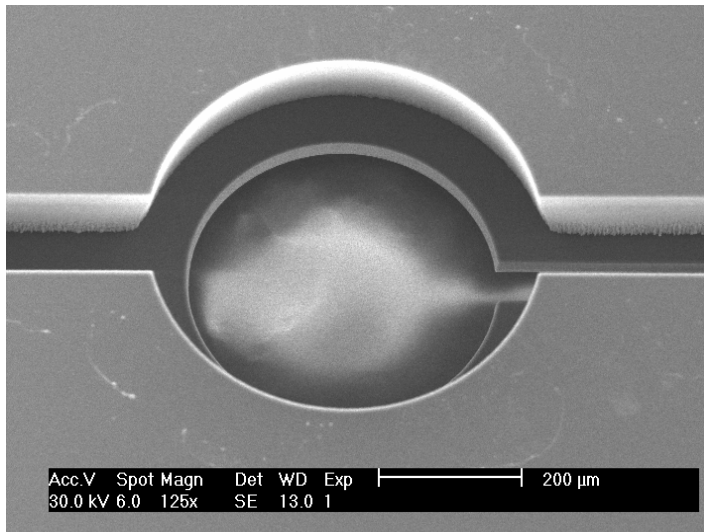
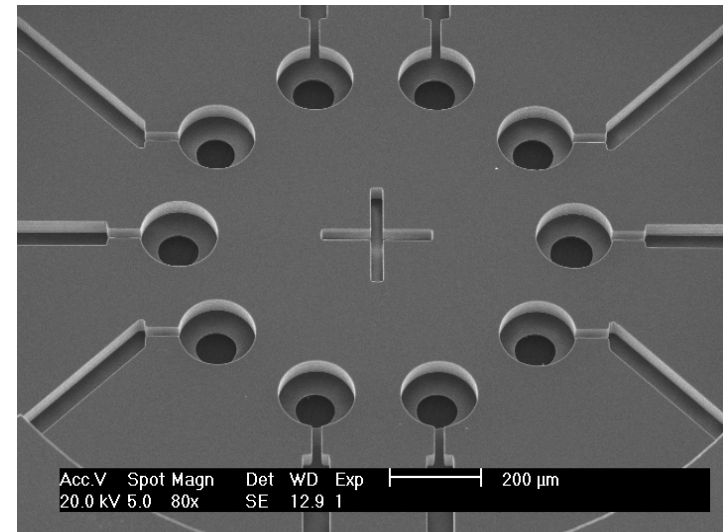


Fig. Thruster assembly with individually addressable extractor electrodes

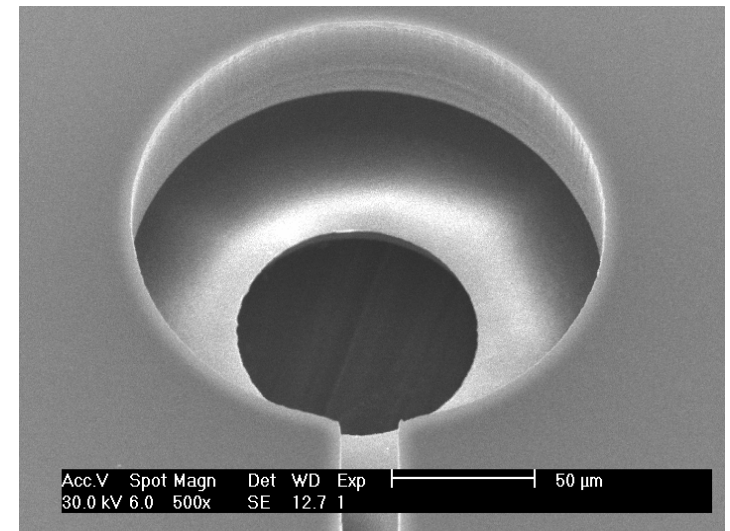
# Microfabrication Extractor



SEM image of wirebonding pad

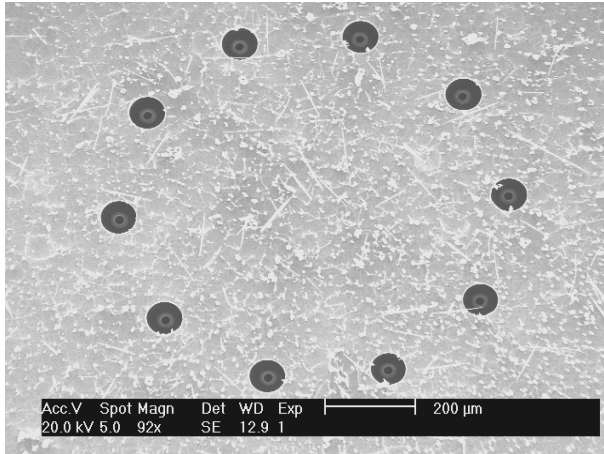


SEM image of extractor electrode array

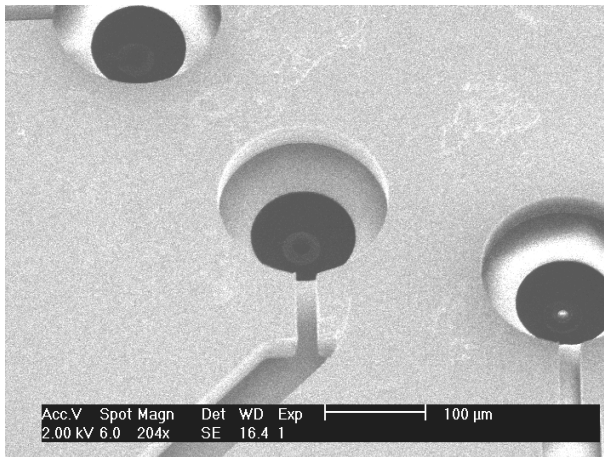


SEM image of extractor electrode

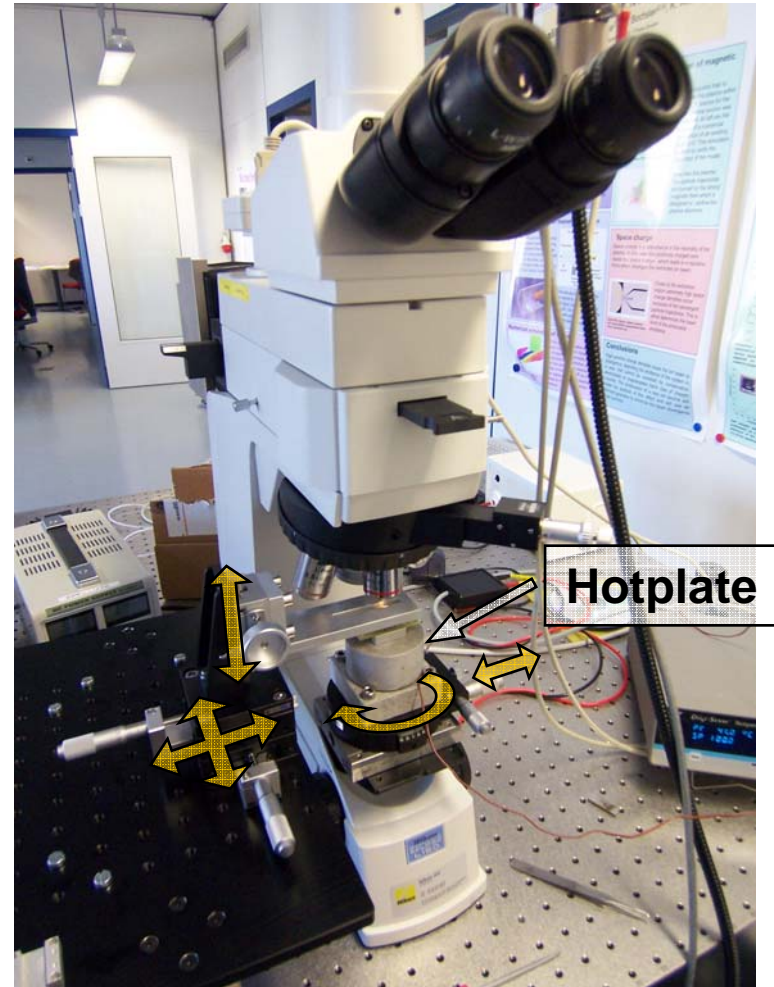
# Microfabrication Assembly



**Fig.** Assembled thruster with simultaneous addressable electrodes

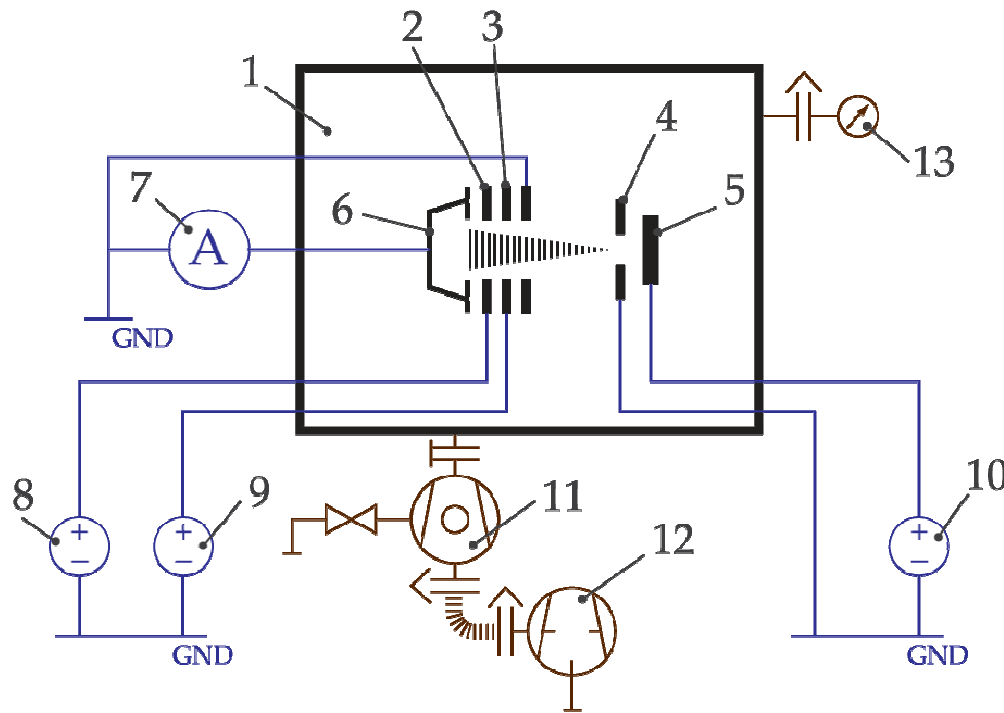


**Fig.** Assembled thruster with individually addressable electrodes



**Fig.** Setup to assemble individual chips below a microscope

# Beam current & energy measurements Test bench – Overview

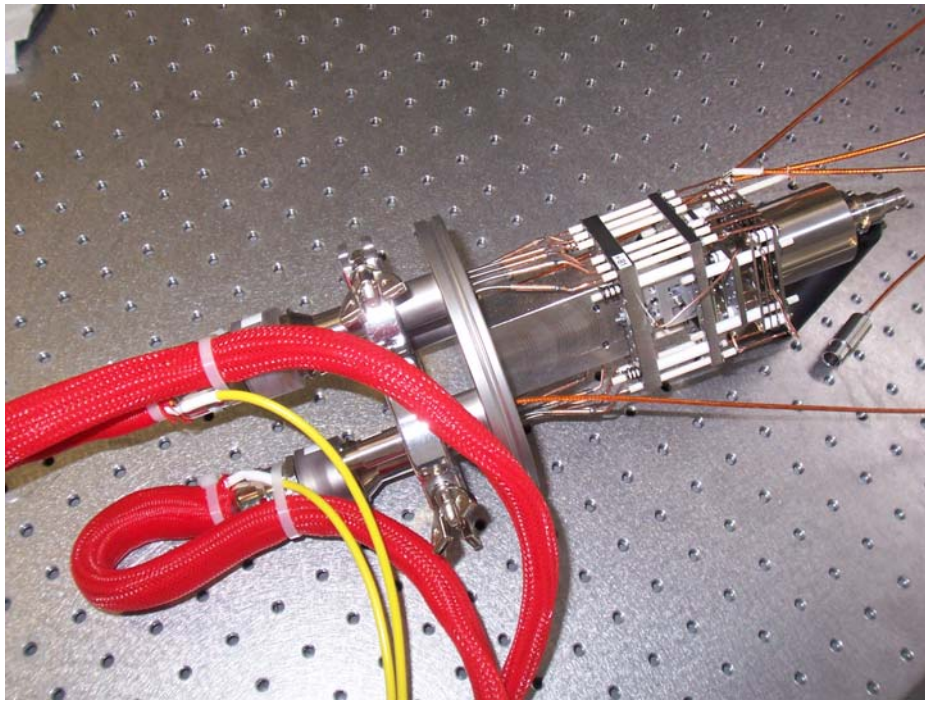


- 1 Vacuum chamber
- 2 Supression Grid
- 3 Retarding grid
- 4 Extractor electrode (on chip)
- 5 Capillary emitter (on chip)
- 6 Faraday cup
- 7 Picoammeter
- 8 Voltage source (supression grid)
- 9 Voltage source (retarding grid)
- 10 Voltage source (emitter)
- 11 Turbomolecular vacuum pump
- 12 Roughing pump
- 13 Pressure gauge

Schematic layout of test setup



## Beam current & energy measurements



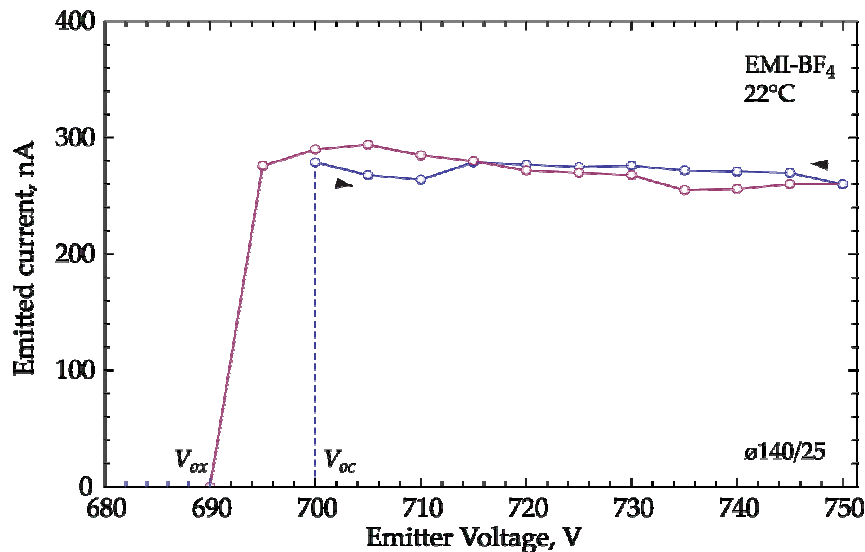
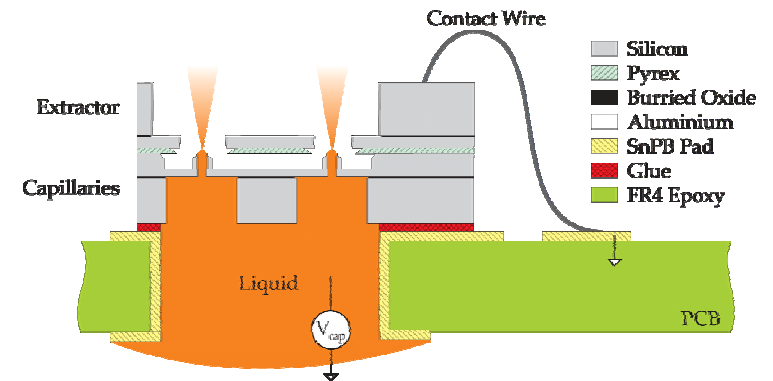
**Fig.** Ion gun with mounted Faraday cup



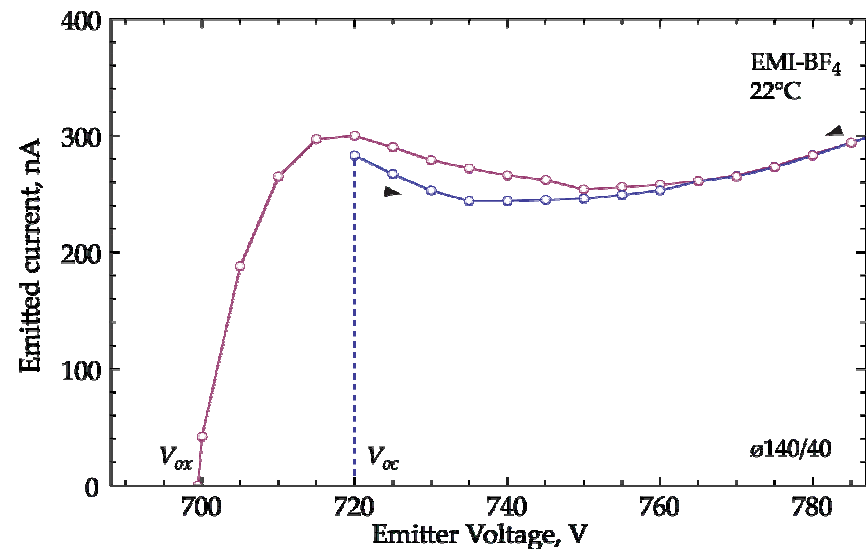
**Fig.** Electro-spray test-rig at EPFL-LMTS

## Current – voltage characteristics Effects of capillary tip to extractor distance

- Current-voltage measurements for a single capillary.



(a)

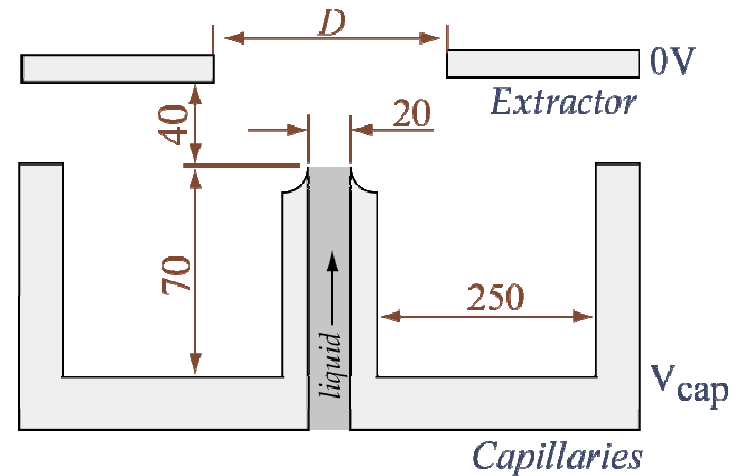
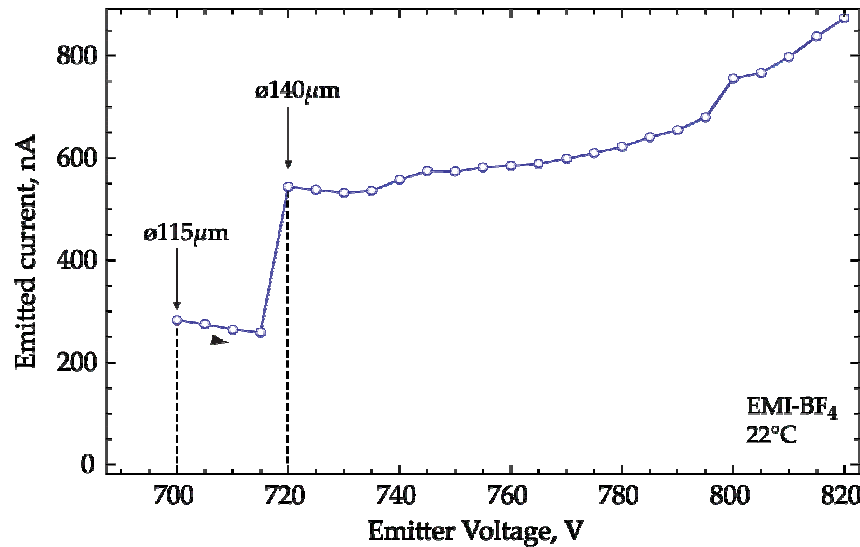
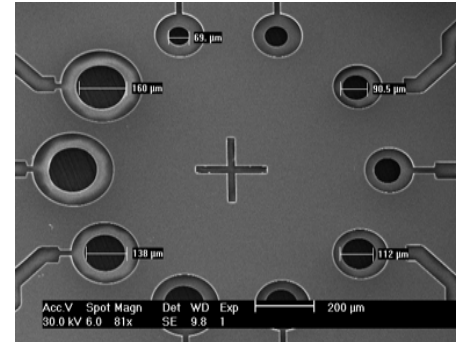


(b)

Current-voltage curve for a capillary with a  $20\mu\text{m}$  i.d. and  $140\mu\text{m}$  diameter electrodes spaced at (a)  $25\mu\text{m}$  and (b)  $40\mu\text{m}$  from the emitter

## Current – voltage characteristics Extractor diameter variation

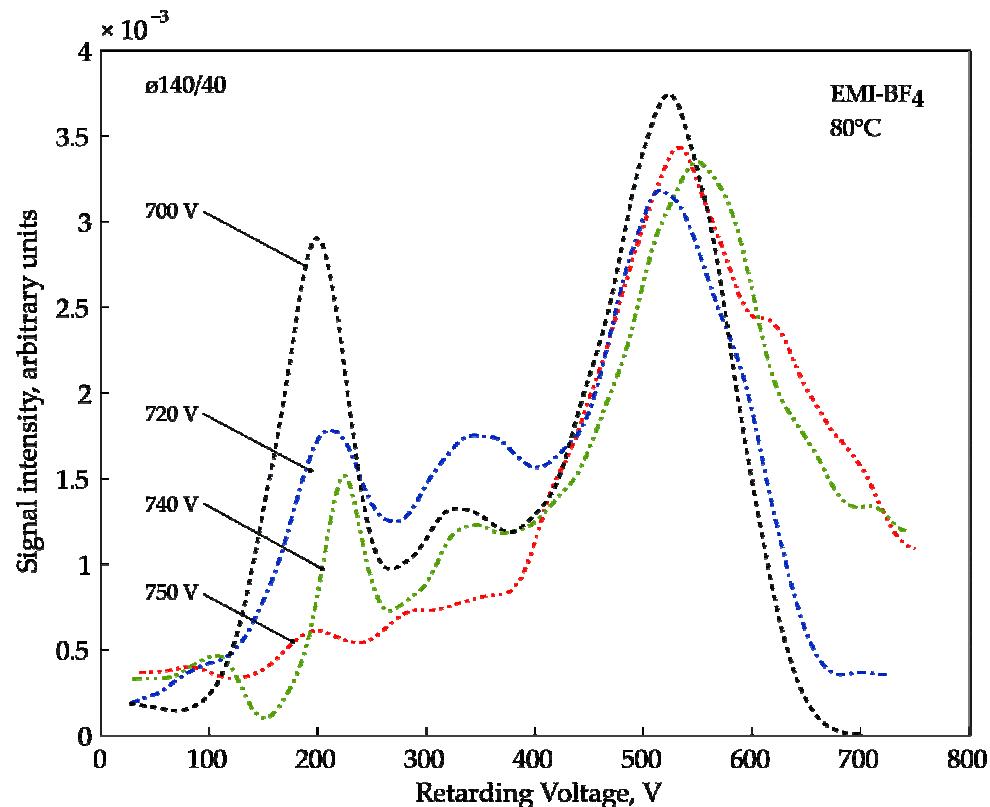
- Thrust modulation can be achieved by varying the extractor diameter



Current-voltage curve for a capillary with a  $20\mu\text{m}$  i.d. capillary and an electrode spaced  $40\mu\text{m}$  from the emitter. Two capillaries with different extractor diameters are tested together.

## Retarding potential

- The large energy distribution indicates most likely the presence of a jet and therefore the existence of droplets in the beam.

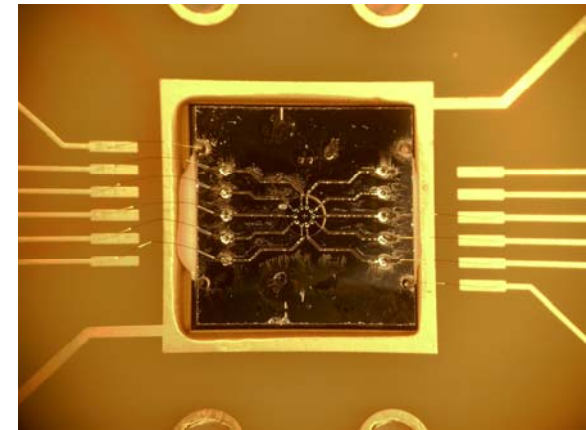


Need to do mass spectrometry to determine different operation modes and hence thrust

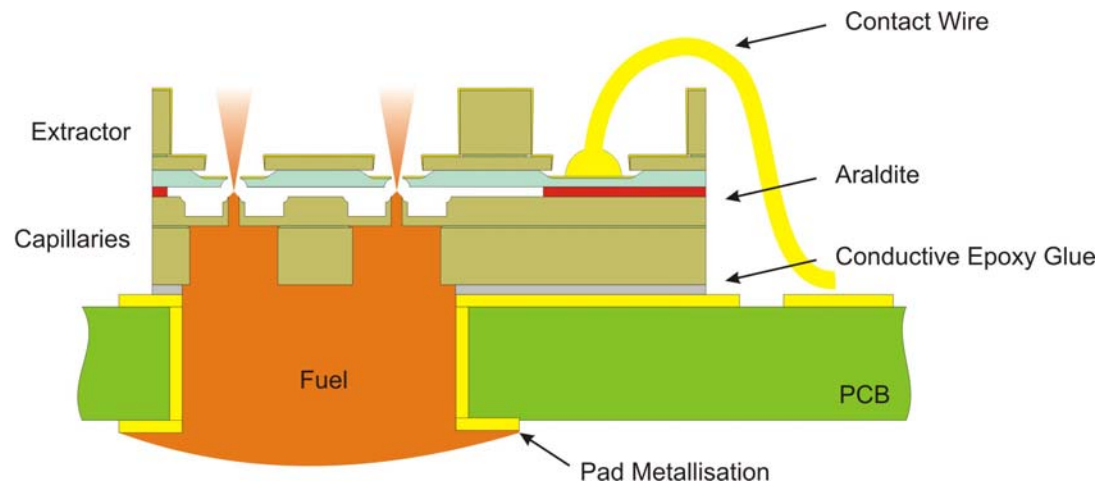
**Fig.** Retarding potential measurement of a capillary with 140µm extractor electrode at 40µm from the emitter. Measurements were taken for different operation voltages.

## Individually addressable chips

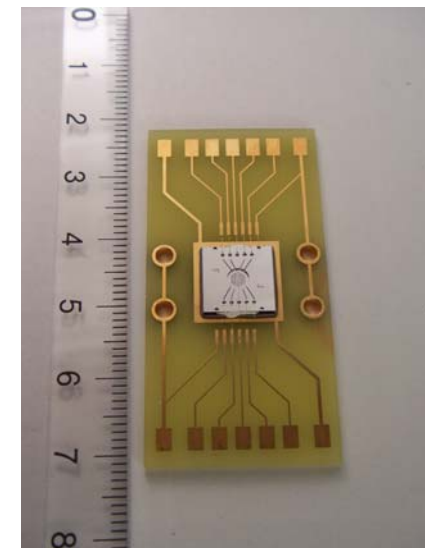
- Stable spraying observed for a few minutes before flooding of the chip.
- Observed current of 150nA for a single emitter at 570V.
- New batch of chips in fabrication to solve identified issues



Detail of assembled thruster



Cross section of a the thruster with individually addressable extractor electrodes



Assembled thruster with PCB support

# Technology Readiness Level

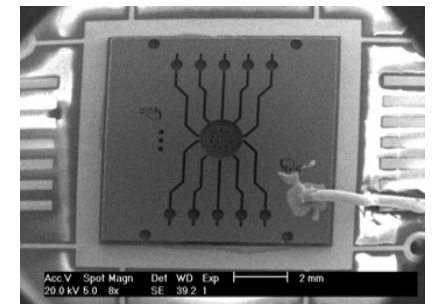
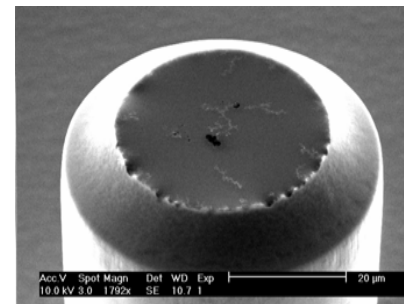
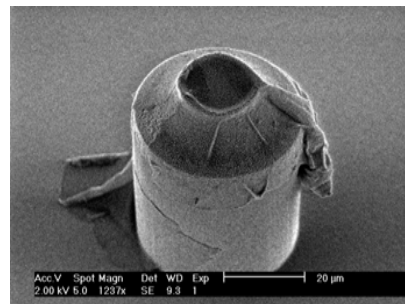
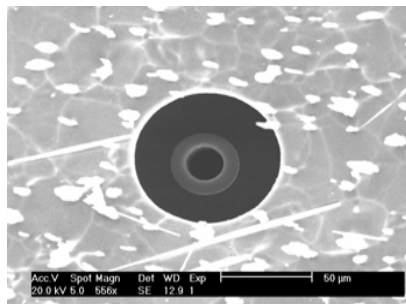
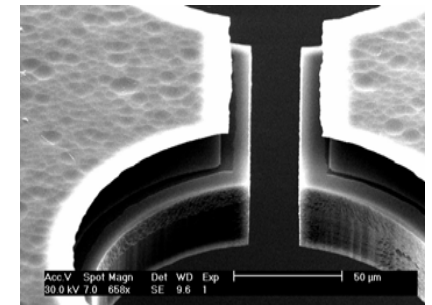
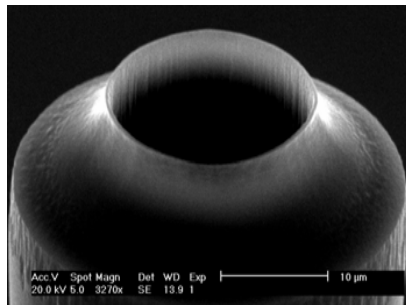
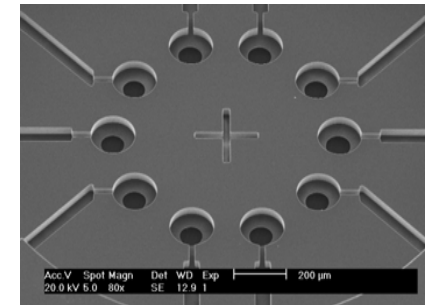
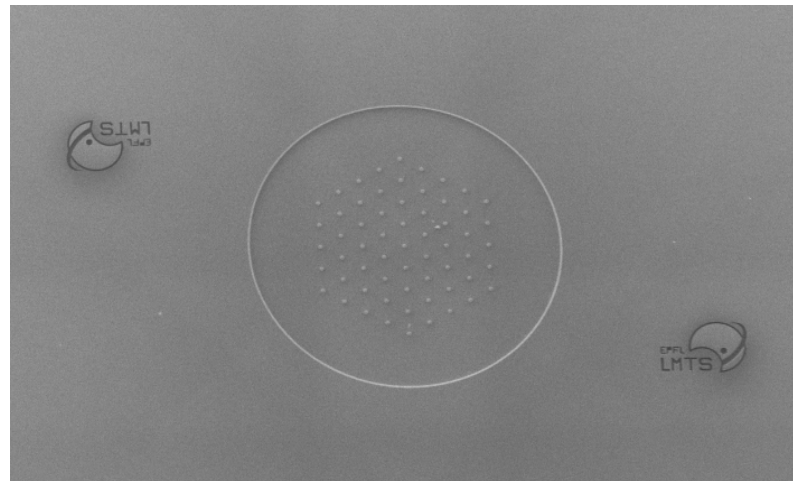
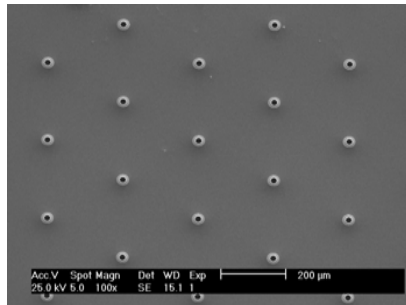
- Current development status is TRL2

| Technology Readiness Levels Summary |   |
|-------------------------------------|---|
| 1                                   | Basic principles observed and reported  |
| 2                                   | Technology concept and/or application formulated  |
| 3                                   | Analytical and experimental critical function and/or characteristic proof-of-concept            |
| 4                                   | Component and/or breadboard validation in laboratory environment                                |
| 5                                   | Component and/or breadboard validation in relevant environment                                  |
| 6                                   | System/subsystem model or prototype demonstration in a relevant environment (ground or space)   |
| 7                                   | System prototype demonstration in a space environment   |
| 8                                   | Actual system completed and “flight qualified” through test and demonstration (ground or space) |
| 9                                   | Actual system “flight proven” through successful mission operations                             |

## Conclusions

- The microfabrication process for a small integrated MEMS electropray thruster has been validated
- Thruster operation has been demonstrated for small arrays, including a new way to obtain thrust modulation.
- A FEM based model to predict the starting voltage of the emission shows a good correlation with the obtained results
- Thruster lifetime remains an unexplored issue. Design improvements such as microchannels at the capillary inlet and chip heating are expected to lead to repeatable capillary filing and spraying.
- We are continuing to develop the thruster in collaboration with partners, and are looking for opportunities to test on nanosatellites

# Questions





## Contact info

R. Krpoun (renato.krpoun@epfl.ch)

H. Shea (herbert.shea@epfl.ch)

Microsystems for Space Technologies Laboratory

EPFL

Rue Jaquet Droz 1

CP 526

CH-2002 Neuchatel

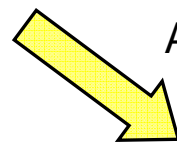
Switzerland

<http://lmts.epfl.ch>

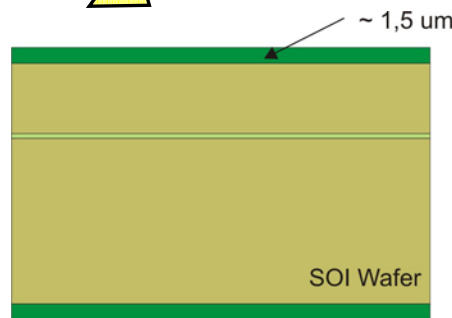
# Microfabrication Capillary Wafer – Process flow (1)



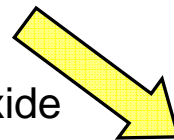
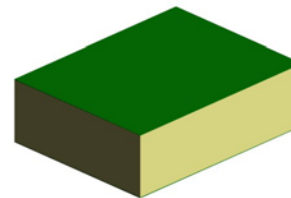
Start with an Silicon-on-Insulator wafer



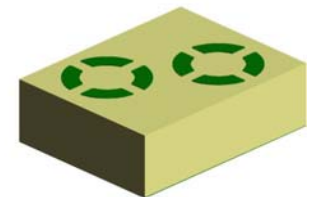
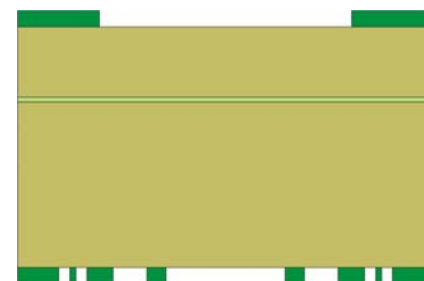
A thermal oxide layer for standoff structures is grown



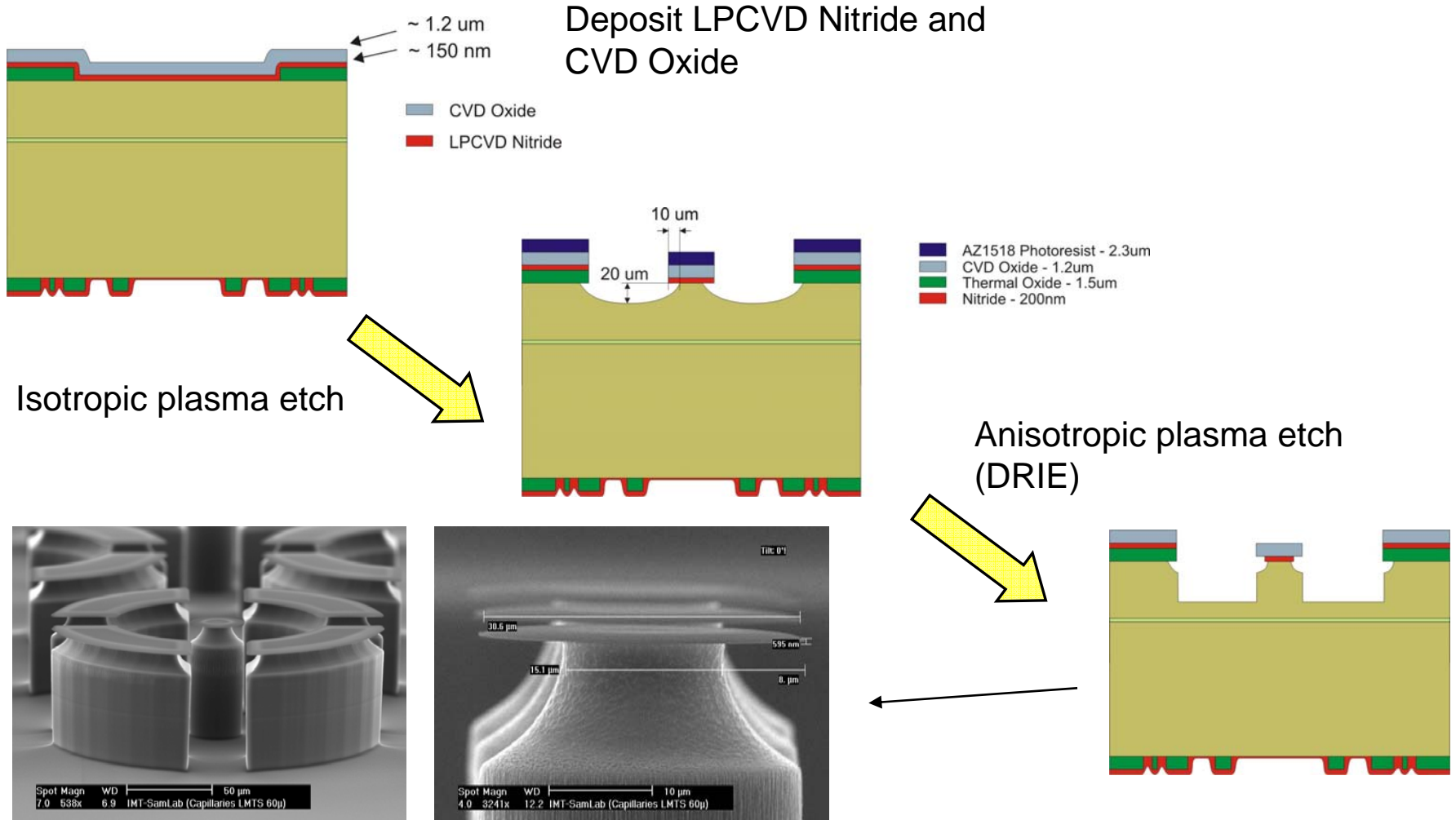
Thermal Oxide  
Buried Oxide



Pattern oxide

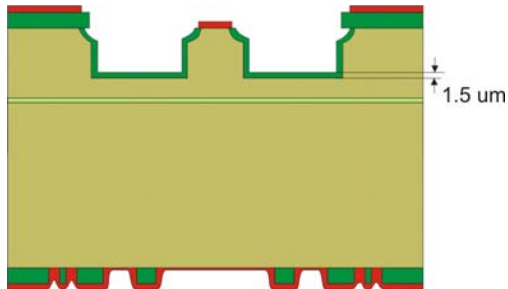


# Microfabrication Capillary Wafer – Process flow (2)

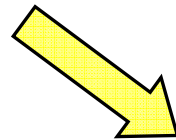


**Fig.** SEM images of capillaries after isotropic/anisotropic etching

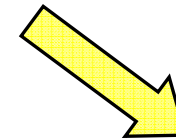
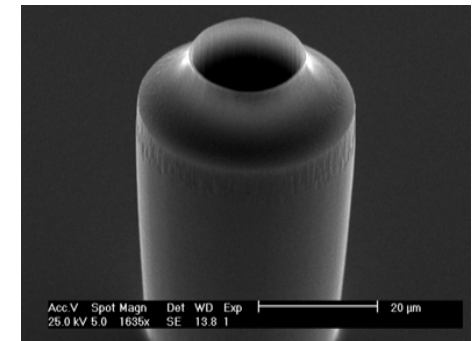
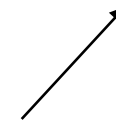
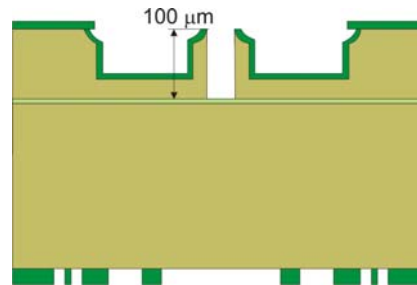
## Microfabrication Capillary Wafer – Process flow (3)



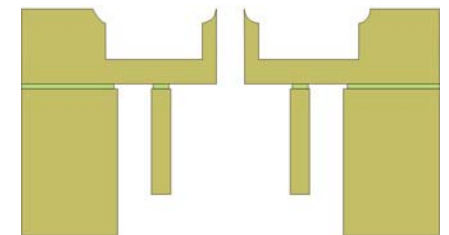
Oxide growth, no oxide will be formed where the silicon is protected by a nitride layer (red)



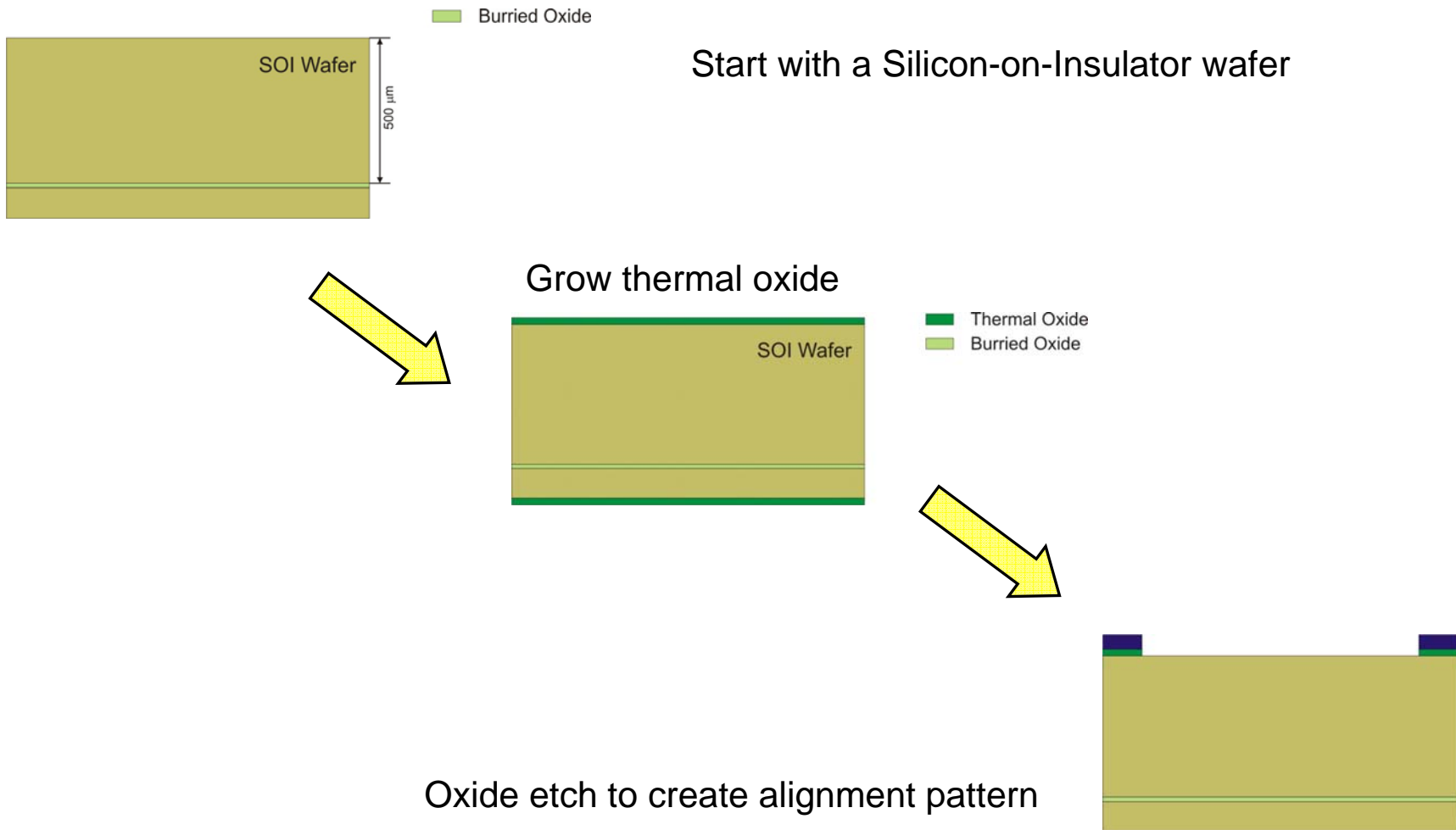
Remove nitride, perform anisotropic plasma etch (DRIE).



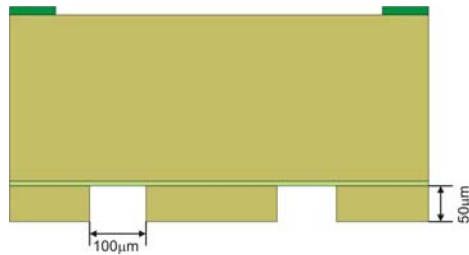
Etch backside (DRIE) and remove oxide by HF vapor etching



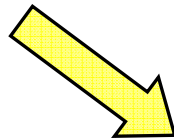
# Microfabrication Extractor – Process Flow (1)



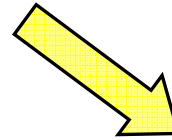
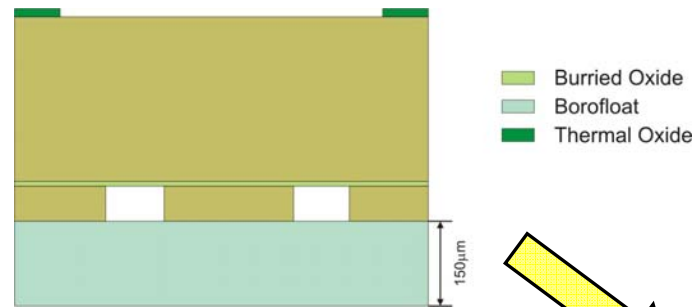
# Microfabrication Extractor – Process Flow (2)



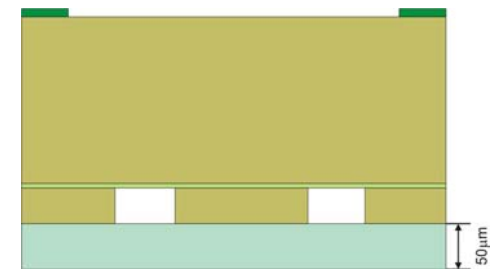
DRIE of shadow mask pattern



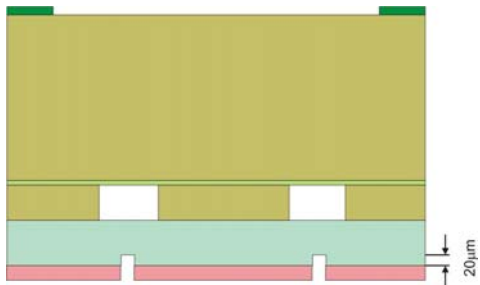
Anodic bonding of Borofloat (Pyrex) wafer



Thinning of Borofloat

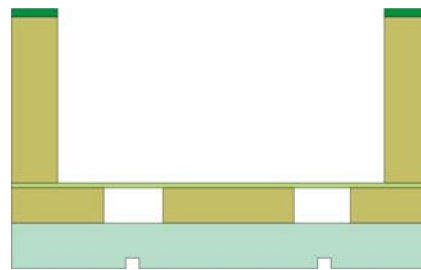


# Microfabrication Extractor – Process Flow (3)

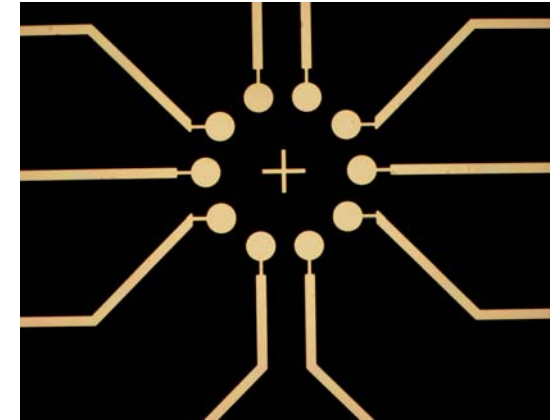
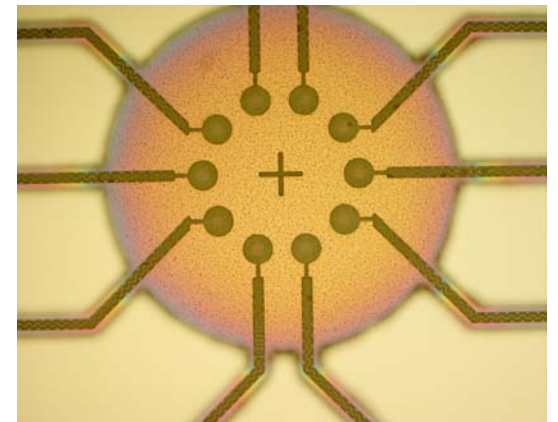


Amorphous silicon deposition, patterning and Pyrex etch  
**(only executed for individually addressable Electrodes)**

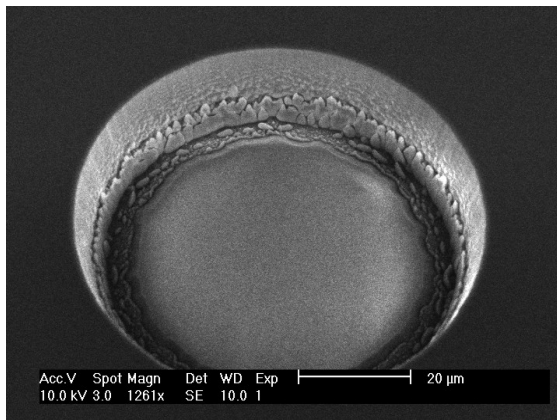
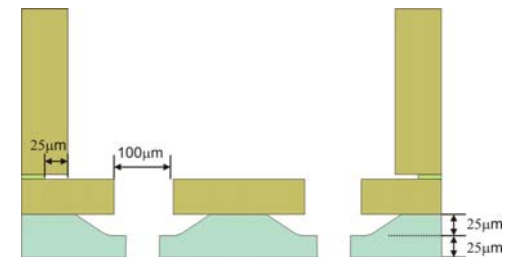
Etch handle layer (DRIE)



HF 20% Pyrex wet etch



**Fig.** Image of extractor electrode array



**Fig.** SEM image of etched Borofloat

## Discussion

### Starting Voltage - Modelling

- Equilibrium between surface tension and electrical stress

$$\frac{1}{2} \varepsilon_0 E_a (V)^2 = \frac{2\gamma}{r_a}$$

$r_a$  – Radius of the cone apex  
 $\gamma$  – Surface Tension  
 $E_a$  – Electric Field at the apex  
 $V$  – Voltage  
 $\varepsilon_0$  – Permittivity of free space

- Linear relation assumed between electric field and applied voltage

$$E_a = \alpha \times V \quad \alpha \text{ – Proportionality factor}$$

- Solving for the voltage yields

$$V_{oc} = \frac{1}{\alpha} \sqrt{\frac{4\gamma}{\varepsilon_0 r_a}}$$

- The proportionality factor,  $\alpha$ , can be determined by FEM analysis



## Discussion Starting Voltage - Correlation

- The proportionality factor,  $\alpha$ , was determined for different apex radii
- Conic section on top of capillary modeled using a rational quadratic parametric equation.
- Results for a  $20\mu\text{m}$  capillary with  $140\mu\text{m}$  diameter extractor, spaced at  $40\mu\text{m}$  from the capillary shown in table below (measured value 720V)

| Tip radius, nm | Critical Voltage, V | $\alpha$ - factor, $\text{m}^{-1}$ |
|----------------|---------------------|------------------------------------|
| 0.6            | 745                 | $7.56 \times 10^6$                 |
| 2.8            | 749                 | $3.56 \times 10^6$                 |
| 12.7           | 751                 | $1.67 \times 10^6$                 |
| 56.8           | 748                 | $0.79 \times 10^6$                 |
| 254.5          | 743                 | $0.39 \times 10^6$                 |
| 1140.6         | 747                 | $0.18 \times 10^6$                 |

Fig. Example plot of the electric field

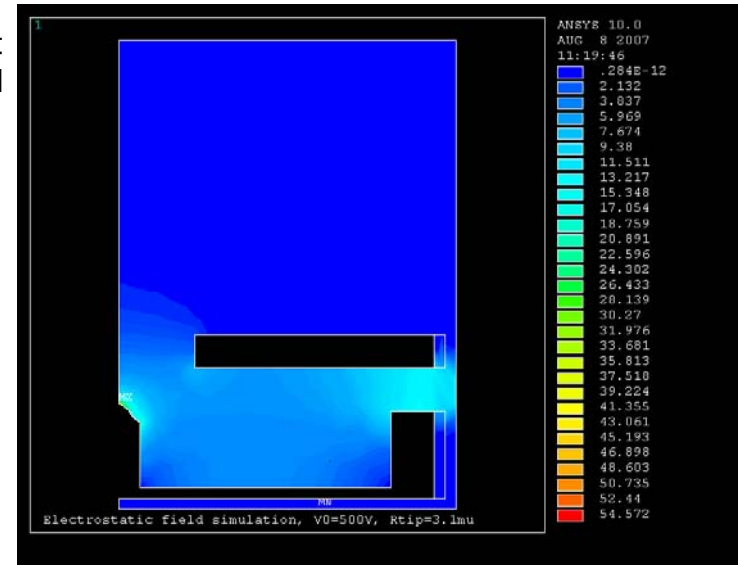


Fig. Example plot of the voltage distribution

