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MEMS based gravity gradiometer for Space Application

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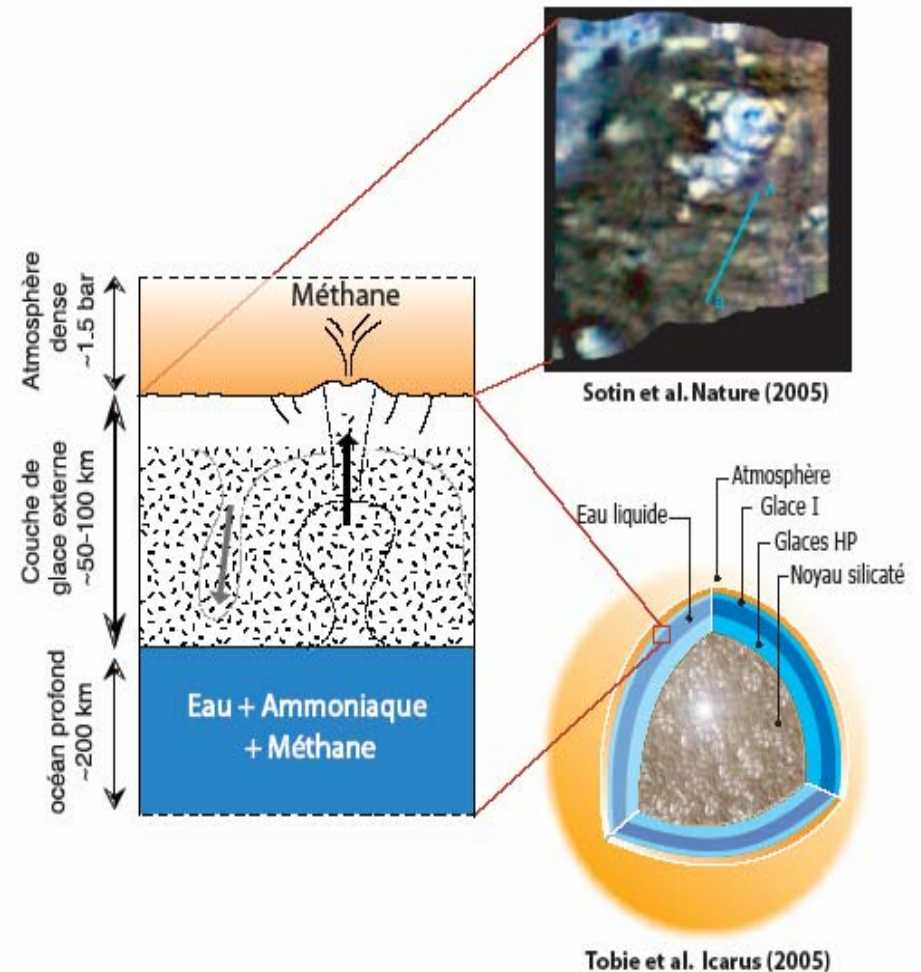


Outline

- Introduction
 - Sensitivity requirements
- Device design
- Sensitivities
 - Brownian / Thermal / Readout
- Conclusions

Gravity research topics

- Planets/moons
 - Local anomalies
 - Evolution of the planet/moon: global structure
- Combination with other measurements





Basic equations

- Gravity potential describes the gravity field
- Differentiating this potential twice yields the gravity gradient as follows:

$$V(r, \theta, \phi) \rightarrow \vec{g} \rightarrow \Gamma$$

- The unit of gravity gradient is Eötvös (E): $1E = 10^{-9}/s^2$
- Gravity potential over a surface is described with spherical harmonics:

$$V(r, \theta, \phi) = \sum_{n=0}^{\infty} \sum_{m=0}^m \frac{GM}{a} \left(\frac{a}{r}\right)^{n+1} \left(A_n^m \cos(m\phi) + B_n^m \sin(m\phi) \right) P_n^m(\theta)$$

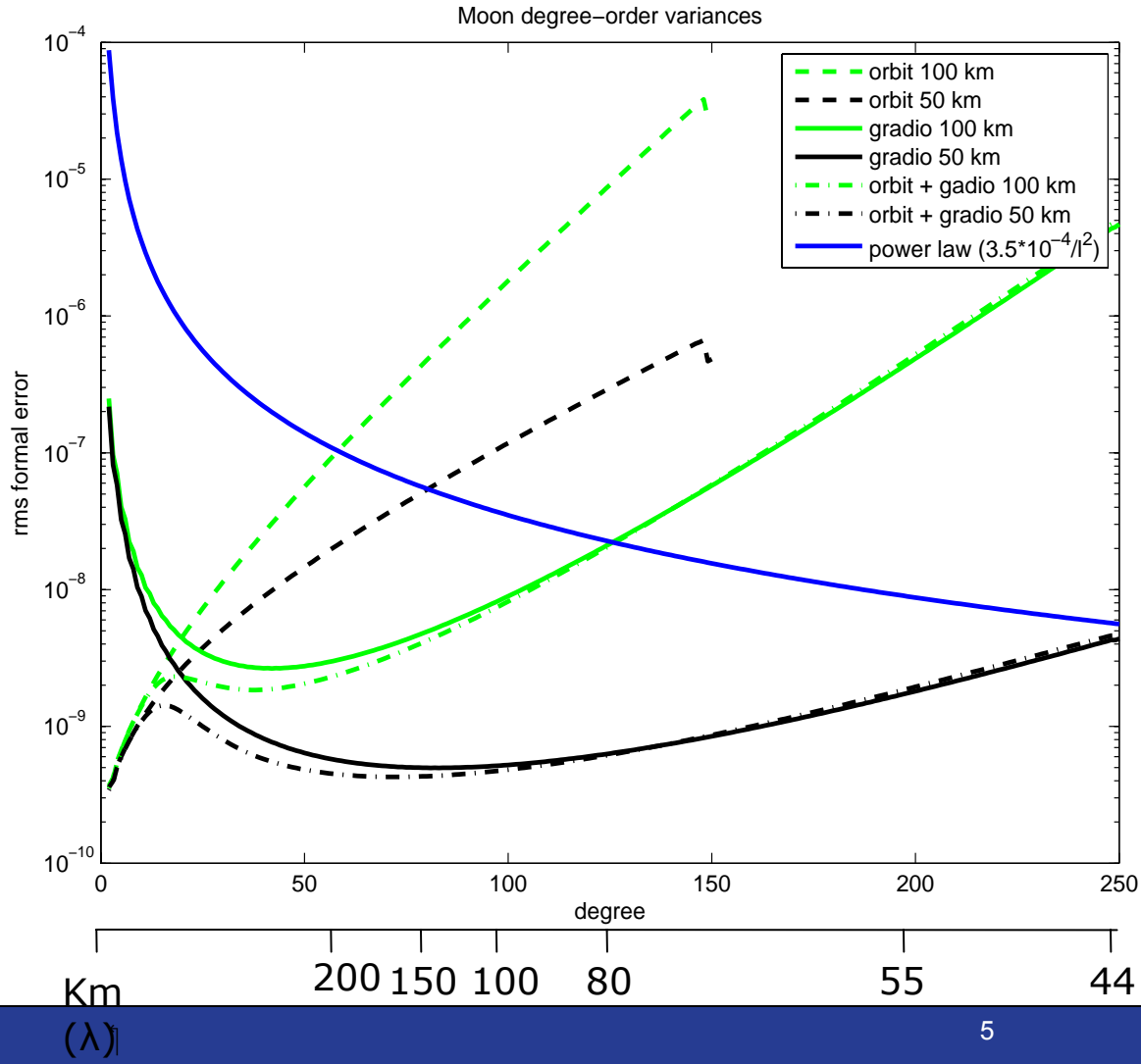
With P the associated Legendre polynomials, n order, m degree

- Higher orders describe the details

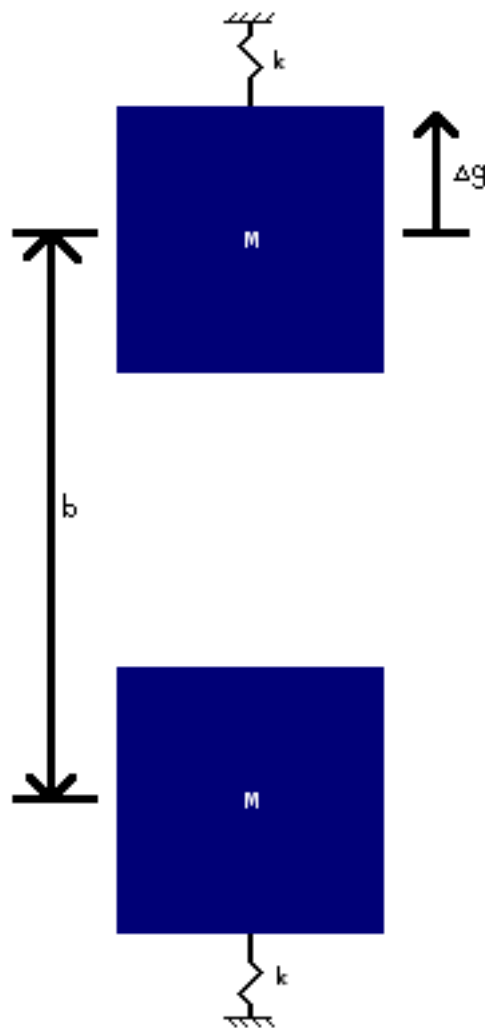
Sensitivities needed for Moon

At least $1\text{E}/\text{rtHz}$
is needed

$T = 1 \text{ yr}$
 1 repeat
 $\sigma_{\text{orb}} = 1 \text{ m}/\sqrt{\text{Hz}}$
 $\sigma_{\text{grad}} = 1 \text{ E}/\sqrt{\text{Hz}}$
 sampling = 1 Hz
 V_{zz} only
 MB = 0.001 - 1 Hz



Power spectral density of gravity gradient sensors



$$S_{\Gamma} = \Gamma_n^2 = \frac{8}{mb^2} \left(\frac{k_b T 2\pi f}{Q(f)} + \frac{(2\pi f_0)^2}{2\beta\eta} \varepsilon_A(f) \right)$$

Here:

b is the base line between the two probe masses

m is the probe mass

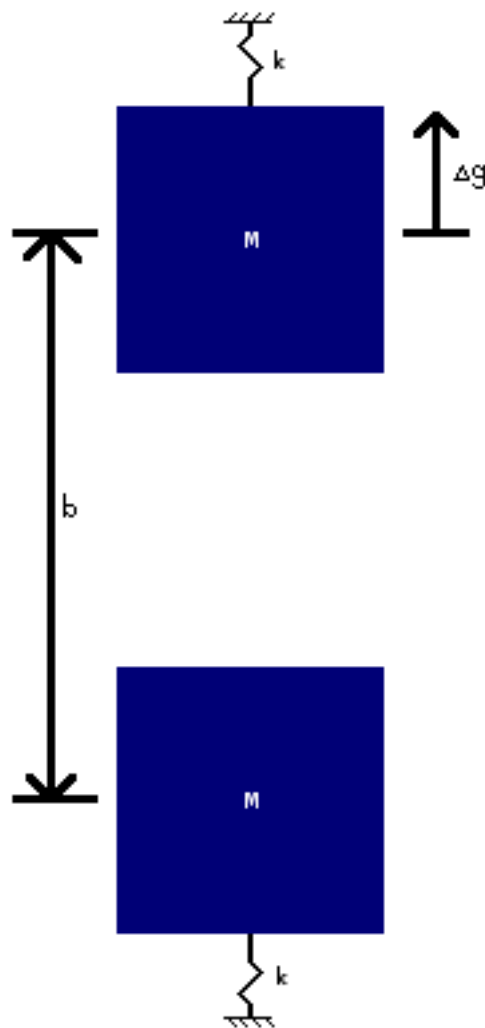
f_0 is the mechanical resonance frequency
of the differential mode

Q is the quality factor of the resonance mode

$\beta\eta$ is the energy coupling factor of the sensor

ε_A is the sensor noise energy

Power spectral density of gravity gradient sensors

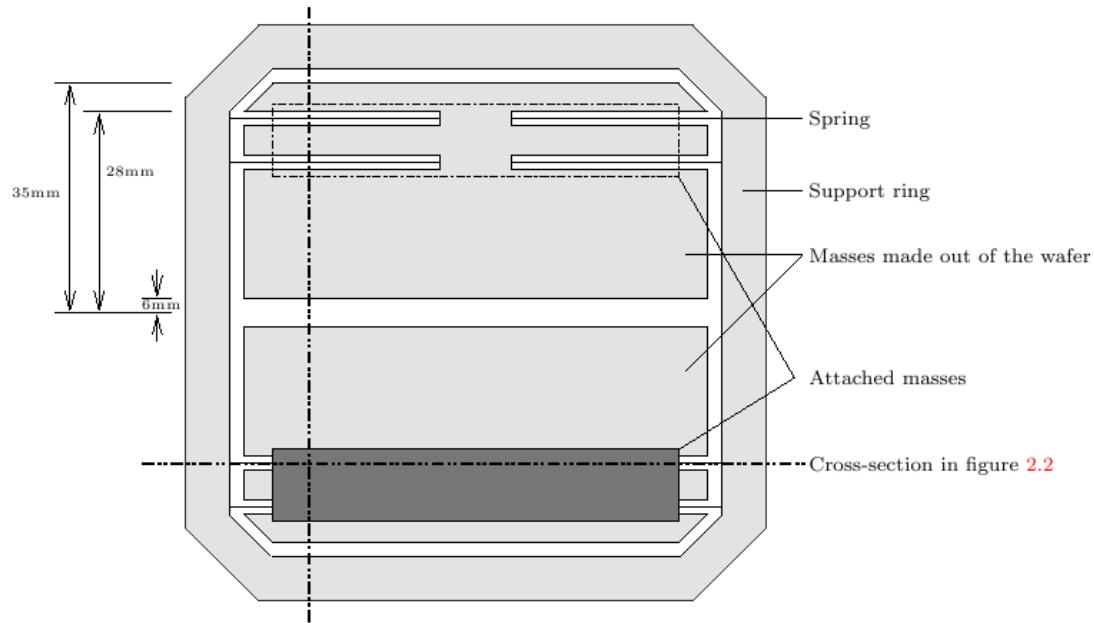


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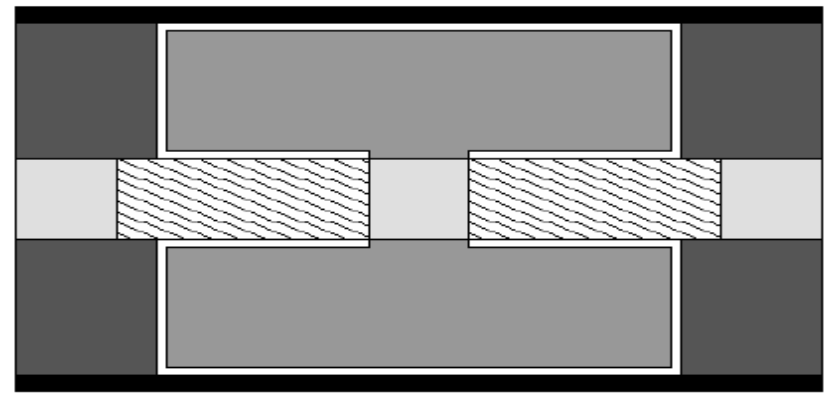
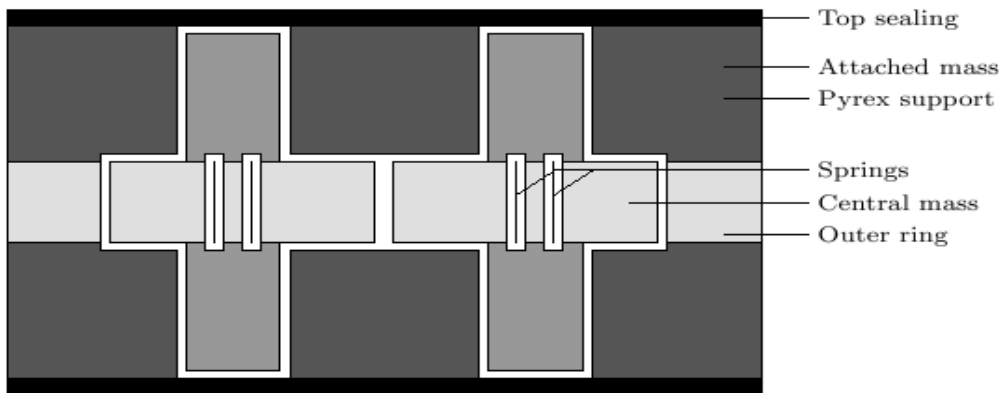
- For a good gradiometer mass and baseline should be big
- For use on a satellite, mass & size must be small

Miniaturization needed --> MEMS

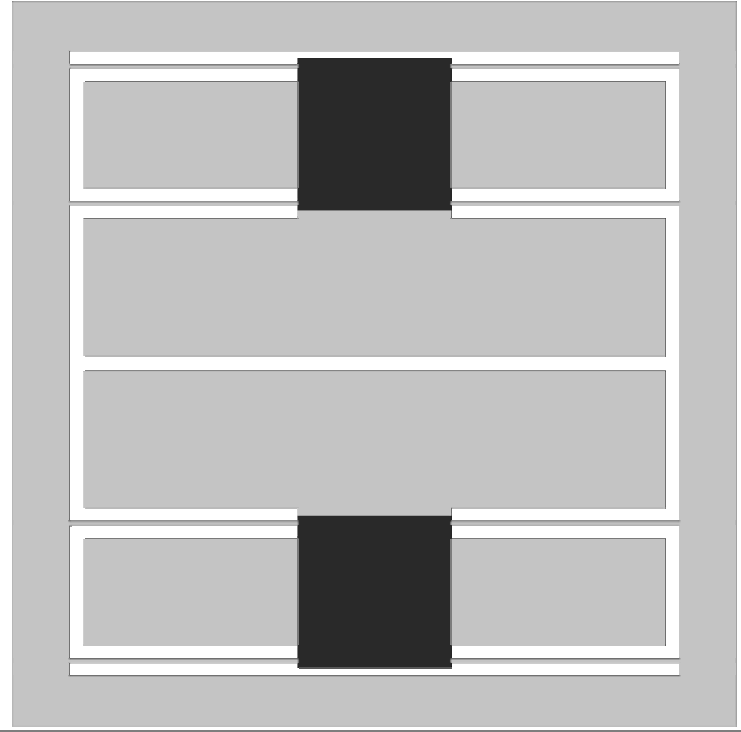
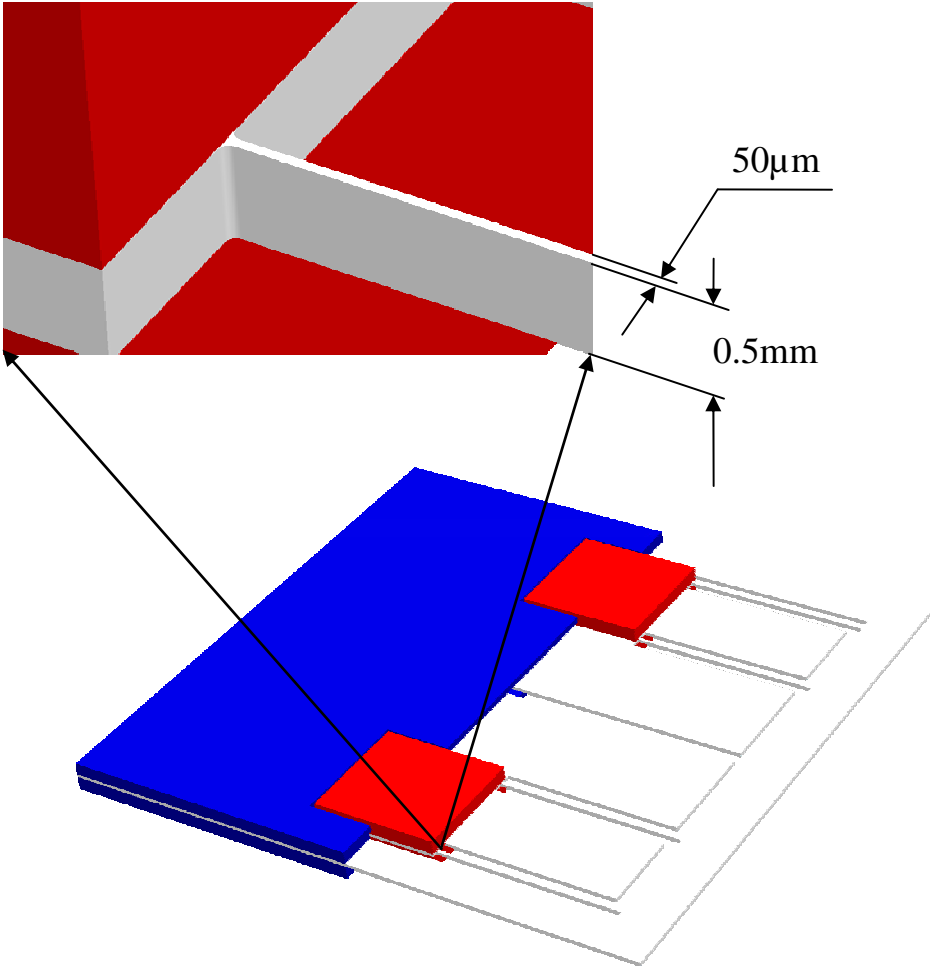
MEMS – Concept design



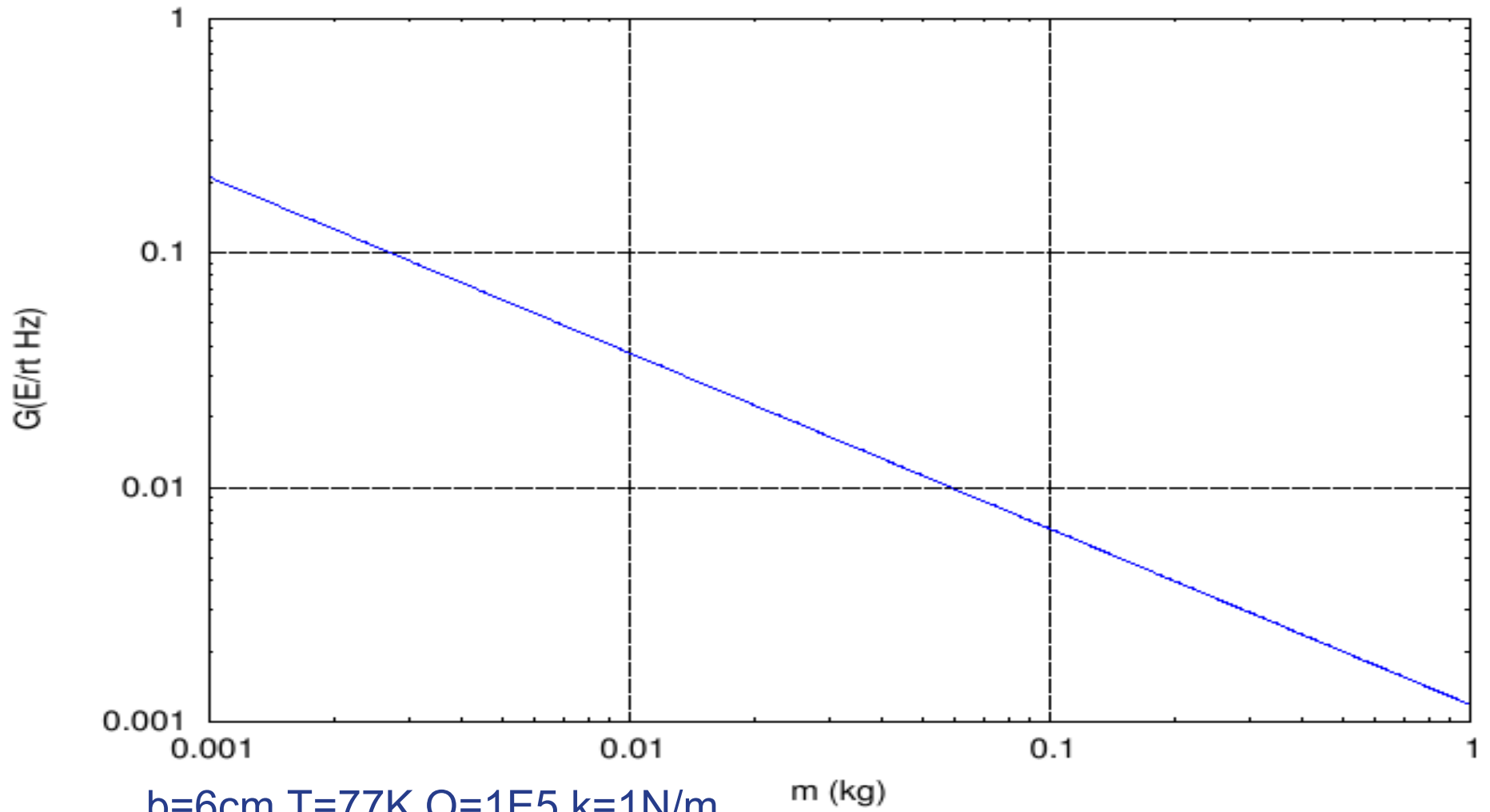
Cross-section in figure 2.3



MEMS – Concept design



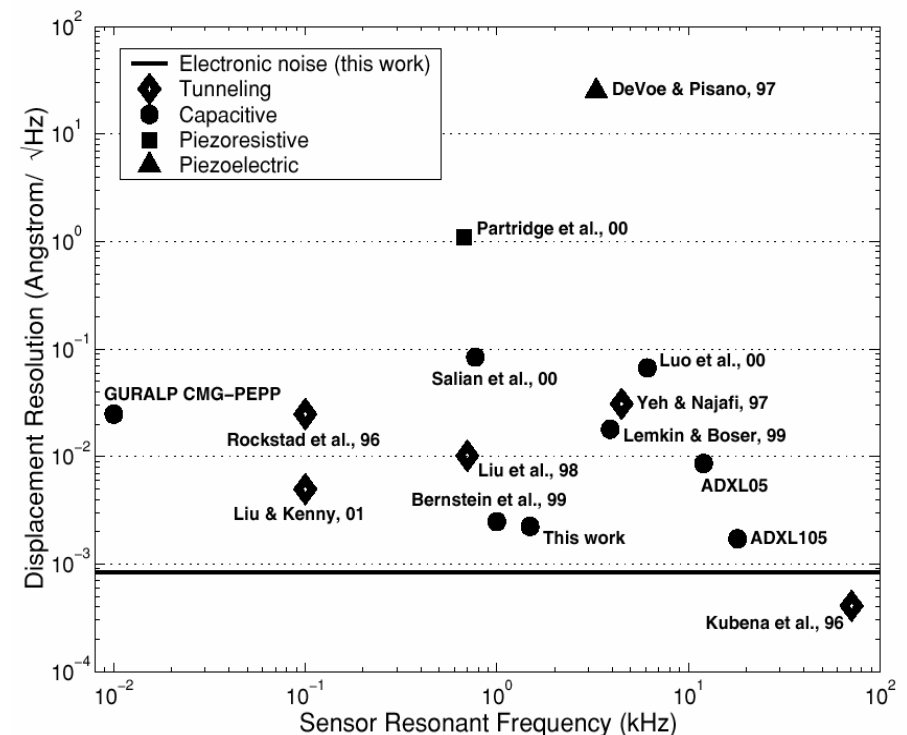
Brownian noise as function of mass with fixed spring constant





Readout – capacitive

- Possibility to detect small deflection has been shown in literature: $10\text{-}13\text{m/s}^2/\sqrt{\text{Hz}}$
- Relative easy integration with mechanics
- Same components for actuation, which means:
 - Readout also applies force to masses!
 - Same type of plates used for force feedback





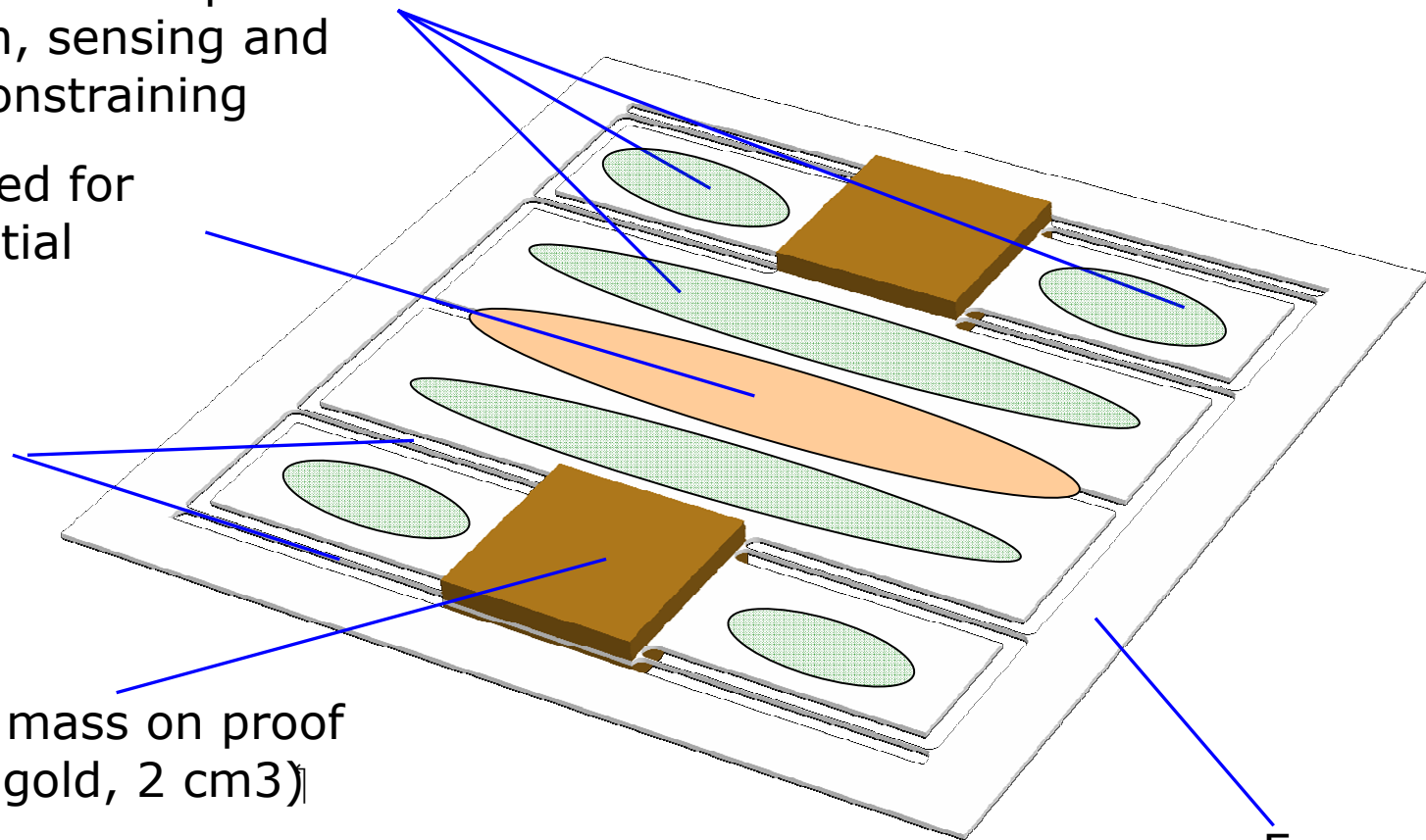
MEMS – Capacitive sensing & actuation

Areas on proof mass designated for capacitive actuation, sensing and lateral constraining

Area designated for direct differential read out

Mechanical constraints (leaf springs)

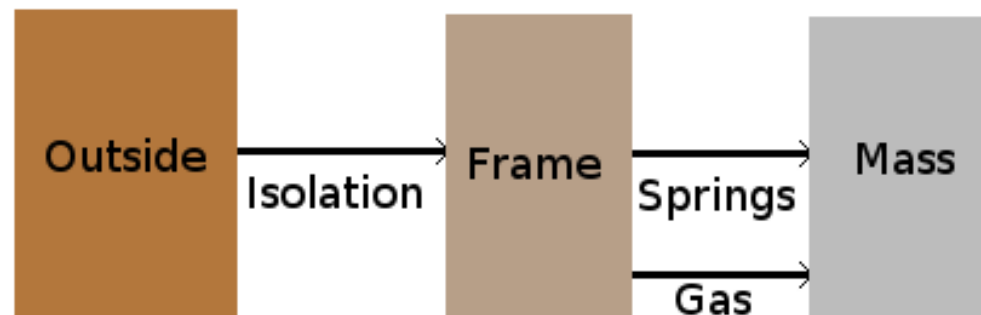
Added mass on proof mass (gold, 2 cm³)





Thermal influences

- “DC” heating of the sensor: $T_{\text{mass}} = T_{\text{frame}}$
 - Everything expands, C change negligible
- Dynamic heating: $T_{\text{mass}} \neq T_{\text{frame}}$
 - Frame moves relative to readout: distance between spring work point and readout is important





Calculation of model

Springs: $l \times b \times h = 6\text{cm} \times 50\mu\text{m} \times 500\mu\text{m}$

$k_x = 500\text{kN/m}$, $k_y = 1.38\text{N/m}$, $k_z = 138\text{N/m}$

2 clamped-clamped-beam springs per acc.meter

Attached mass: Au: $\rho W = 19,300\text{kg/m}^3$

$l \times b \times h = 1\text{cm} \times 1\text{cm} \times 1\text{cm}$

Location: 3.25cm from center of sensor

Mass = 87g



Calculation of model

$Q = 100,000$

Readout: $\Delta x = 10e-13 \text{ m}/\sqrt{\text{Hz}}$

Temperature: $T=77\text{K}$

Total mass: 87g

Frequency: 1Hz

Baseline: 6.4cm



Calculation of model

Results:

Brownian $107\text{mE}\sqrt{\text{Hz}}$

Readout $53\text{mE}\sqrt{\text{Hz}}$

Total $119\text{mE}\sqrt{\text{Hz}}$

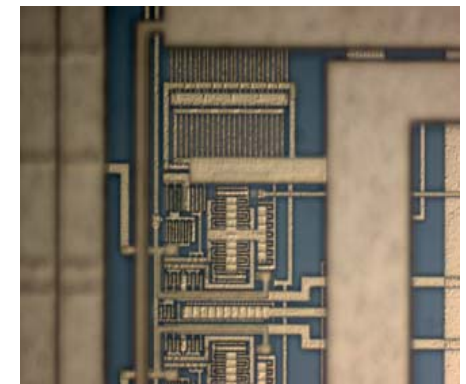
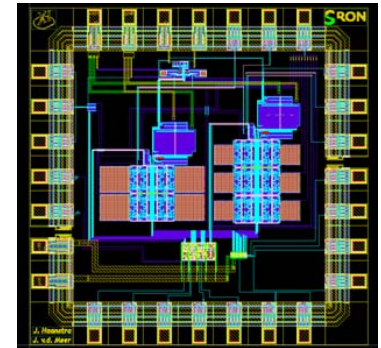


Electronics

Goal:

- Acquiring differential capacitance values
- Processing to get accelerations and gradients
- Providing feedback control to keep masses in workpoints
- Compensate for unmatched systems by using electronic negative springs

Electronics will be developed as ASIC
(Application Specific IC) by SRON





Conclusions

- For planetary missions: at least $1\text{E}/\sqrt{\text{Hz}}$ sensitivity needed
- Proposed design: $119\text{mE}/\sqrt{\text{Hz}}$ possible
- Systems need to equal to reject common mode accelerations
 - Negative spring constants can be used to control